# U.S. DEPARTMENT OF THE INTERIOR U.S. GEOLOGICAL SURVEY

Seismic velocities and geologic logs at seven strong-motion stations that recorded the 1989 Loma Prieta, California, earthquake, Part IV

by

James F. Gibbs and Thomas E. Fumal <sup>1</sup>

### Open-File Report 94 - 552

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#### INTRODUCTION

The Loma Prieta earthquake of October 17, 1989 (1704 PST) was recorded at 131 strong-motion stations located through-out the San Francisco Bay area (Maley et al., 1989, Shakal, et al., 1989). This data set has enormous value for engineering and seismological studies regarding earthquake ground motions. Using damage to man-made structures from the 1906 San Francisco earthquake, Wood (in Lawson, chairman,1908) recognized that ground-motion intensity could be correlated with differences in local site geology. In order to quantify the effect of local geology (e.g., Borcherdt, 1970; Borcherdt and Gibbs, 1976; Borcherdt and Glassmoyer, 1992) on ground motions from the 1989 earthquake, detailed geologic and geophysical data are needed. To plan the acquisition of these data a meeting was held on July 6, 1990 at the USGS in Menlo Park, California. Eighteen scientists and engineers representing thirteen institutions attended the meeting to coordinate drilling and data aquisition plans at strong-motion stations.

This is the forth in a series of four reports (Gibbs et al., 1992, 1993, 1994) detailing the results of borehole measurements at strong-motion stations recording significant ground motions during the 1989 Loma Prieta earthquake. This report contains the results of the field effort by the USGS for the following seven boreholes located near strong-motion stations operated by the U.S. Geological Survey (Figure 1).

- 1. Anderson Dam (downstream)
- 2. Calaveras Reservoir
- 3. Callens Ranch
- 4. Hollister Airport
- 5. Sunol Fire Station
- 6. Williams Ranch
- 7. Webb Ranch

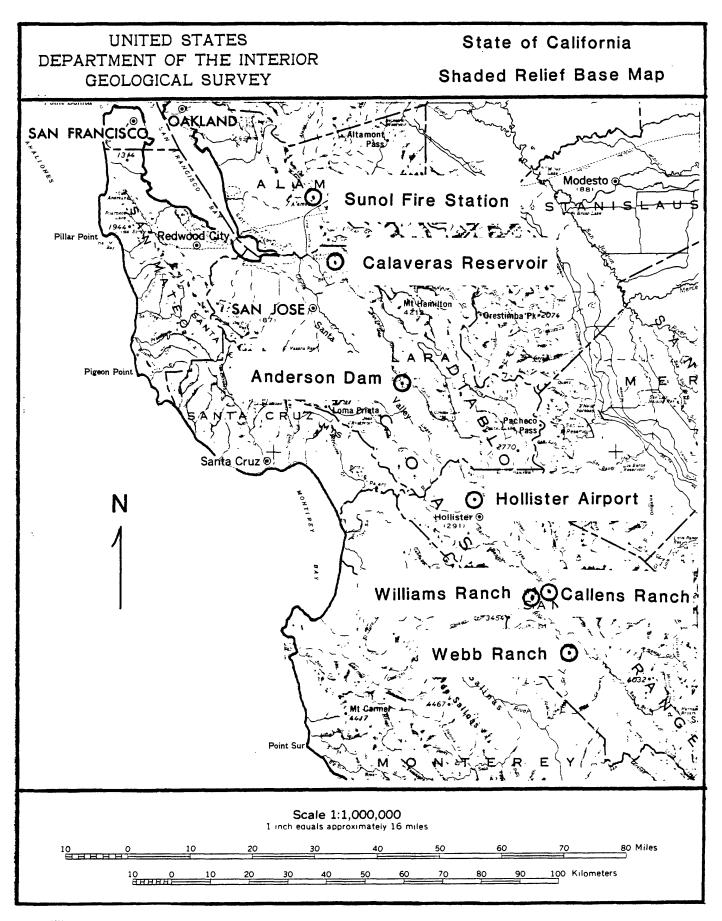


Figure 1. Regional map showing the locations of boreholes (center of circles) included in this report.

#### FIELD MEASUREMENTS

## **Drilling and Sampling Procedures**

Boreholes were located as close as possible to the accelerograph stations that recorded the strong-motion from the Loma Prieta Earthquake. In the case of Anderson Dam, Calaveras Reservoir, Sunol Fire Station, and Webb Ranch the boreholes were drilled approximately 30 meters from the strong-motion instrument. Callens Ranch and Hollister Airport borehole were located within 20 meters of the instrument and Williams Ranch borehole was within 10 meters of the strong-motion accelerograph.

At each site a hole approximately 6 to 10 inches in diameter was drilled using rotarywash drilling with bentonite mud. For purposes of economy, samples were not taken in any of the boreholes.

The borings at all stations in this report were cased with 3-inch inside-diameter, class 200, polyvinyl-chloride pipe capped at the bottom.

The annular space around the casing was tremie grouted by pumping a water-cement-bentonite mixture through a 1-inch steel pipe inserted next to the casing. This provides good coupling between the casing and the wall of the borehole, and provides a sanitary seal preventing contamination of ground water. Grouting was done in stages of about 50-60 meters to prevent collapse of the casing.

#### Geologic Logs

Geologic logs are based on descriptions of drill cuttings, samples, reaction of the drill rig, and inspection of nearby outcrops. Sediment samples are described using the field techniques of the Soil Conservation Service (1951). Descriptions include sediment texture, color, and the amount and size of coarse fragments. Texture refers to the relative proportions of clay, silt, and sand particles less than 2 millimeters in diameter. This is determined visually and by feel without using laboratory tests. As such, this system is easier to use in the field than other classification systems. The dominant color of the sediment and prominent mottles are determined from the Munsell soil color charts.

Descriptions of rock samples include rock name, weathering condition, color, grain size, hardness, and fracture spacing. Classifications of rock hardness and fracture spacing are those used by Ellen et al., (1972) in describing hillside materials in San Mateo County,

#### California.

Most information needed for describing relatively well-sorted soils and such properties of rock as lithology, color, and hardness are readily obtained from cuttings. Inspection of samples and nearby outcrops is necessary for determining the nature of poorly-sorted materials and fracture spacing. Reaction of the drill rig is useful in determining approximate sediment texture and in determining degree of fracturing because the rate of penetration in rock is highest for very closely fractured and crushed materials and drilling roughness generally is at a maximum in closely to moderately fractured rock. In-situ consistency of soil is determined largely from standard penetration measurements and rate of drill penetration.

#### S- and P-wave Data

Shear waves \* were generated at the ground surface by an air-powered horizontal hammer (Liu, et al., 1988) striking anvils attached to the ends of a 2.3-meter-long aluminum channel. The hammer can be driven in both horizontal directions to generate positive and negative shear pulses. The switch that determines zero time is a piezo-electric sensor attached to the shear source. The source is offset from the borehole to prevent the direct arrival from traveling down the grout next to the casing. The source offset is 2 to 5 meters depending on the depth of the borehole. Shallow holes (30 meters or less) are generally offset 2 meters, while boreholes deeper than approximately 100 meters are offset 5 meters. Travel times are corrected (for slant offset) to vertical by the cosine of the angle of ray incidence.

P-waves are made by striking a steel plate with a sledge hammer at the same intervals described above. The recorder is triggered by the sledge hammer making electrical contact with the steel plate.

Measurements are made by lowering a single three-component geophone into the borehole and clamping it to the casing-wall with an electrically-actuated lever arm. A second three-component geophone is placed at the surface approximately 30 centimeters from the shear source and is used as a check of the zero time determined by the triggering of the

<sup>\*</sup> In this report S-wave and shear-wave are used interchangeably as well as P-wave and compressional-wave.

recorder by the contact switch. After the measurement at the bottom of the borehole all measurements for this group of stations were made at 2.5 meter intervals. The data are recorded on magnetic tape cassettes in digital form on a twelve-channel recording system.

#### DATA INTERPRETATION and PROCESSING

The flow-chart, Figure 2, describes the processing and interpretation procedures. The magnetic tape cassette contains 18 recorded traces from each depth. These include data from the surface three component geophone and the downhole three-component geophone. There are a total of 6 traces for each source type (positive horizontal, negative horizontal, and vertical). As mentioned previously, the surface geophone is used only to check timing.

The orientation of the downhole geophone cannot be controlled when moving from one depth to the next, so that horizontal components are not generally oriented parallel and perpendicular to the source. This causes slight phase shifts, timing differences and amplitude variations. To minimize these effects, when timing shear-wave arrivals, the horizontal components are combined (rotated) to obtain a single component of motion. The direction of motion is determined by maximizing the integral square amplitude within a time interval containing the shear wave (Boatwright et al., 1986). Rotated traces are plotted on a 20-inch computer monitor and the first shear-wave arrival is timed for each of the horizontal rotated traces. Two arrival times are obtained from picks of the first S-wave arrival from oppositely directed horizontal impacts. Timing of the arrivals is done to one millisecond precision. The two time-picks are not always identical, due to interfering waves obscuring the first shear-arrival, slight phase shifts, or amplitude differences. If the time difference is greater than about 5 milliseconds a mistake in phase correlation (perhaps due to a reversed trace, noise etc.) can be suspected and a repick may be necessary. The two picks are averaged for velocity determinations. On clear traces one-millisecond picking accuracy can be maintained; however, because of lower signal-to-noise ratios and interfering waves in the deeper sections of the boreholes, this accuracy cannot always be achieved. In the inversion for shear-velocity the arrivals are weighted by the inverse of an assigned normalized variance. A normalized standard deviation of 1 was assigned to the accurate picks and values ranging up to 5 were assigned to the others.

For determining the final velocity model there are a number of ways to proceed. In

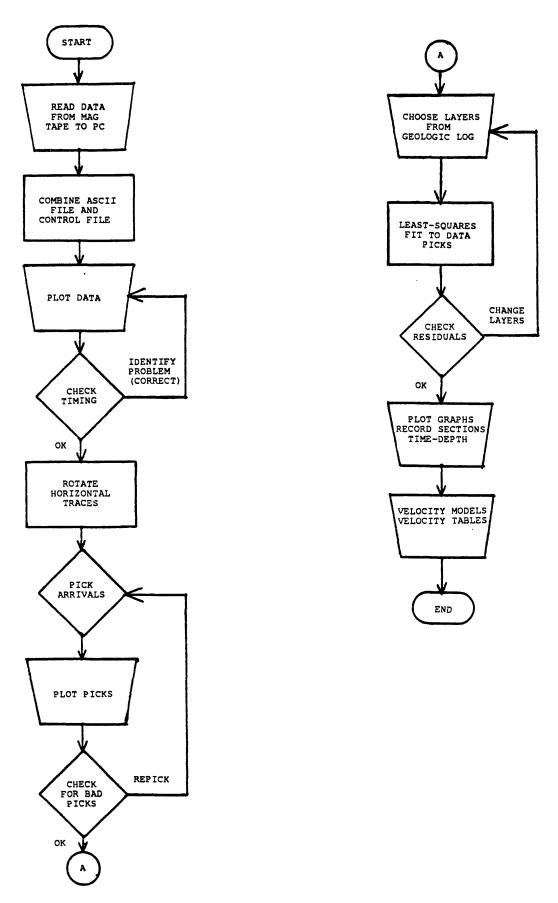


Figure 2. Flow-chart outlining the data processing and interpretation steps.

our earilier work (e.g., Gibbs et al., 1975) we determined the initial layer boundaries from the travel time plots by eye and then added or subtracted layers based on geologic boundaries consistent with the data. We also required at least three data points in each layer. This requirement limited the velocity determination to layers greater than 7.5 meters in thickness. The problem with this proceedure is that a mismatch (overlap or underlap) of the line segments sometimes occurred at the intersections of the layers, resulting in a discontinuous travel time curve. To address this problem we are now using a least-squares program (LFIT, Press et al., 1992) that fits the travel time data with line segments hinged at each selected layer boundary from the surface (forced through zero) to the bottom data point. Initial layer boundaries are chosen from the geologic log and are adjusted, if necessary, to reduce residuals and for consistency with the data. The S-wave travel time data are analyzed first; layer boundaries are initially the same for the P-wave model, and are then adjusted, if necessary, by adding a layer for the water table or reducing the number of layers. The velocity plots (e.g., Figure 13) show upper and lower bounds which approximate 68% confidence limits. These bounds are not symmetrical because they are based on the standard deviation of the slope of the least-squares line fit to the travel time plots (the inverse of the velocity).

#### SUMMARY OF RESULTS

#### S-wave velocities

Figure 3 summarizes S-wave velocities at four sites Anderson Dam, Calaveras Reservoir, Callens Ranch, and Sunol Fire Station. In general, the upper sections at Calaveras Reservoir, Callens Ranch and Sunol Fire Station have similar velocities in thin layering with varing amounts of sand-clay-loam. Anderson Dam has a slightly higher velocity from the surface to 2.5 and then below that a higher velocity layer (543 m/s gravely-sandy-loam) to 25.6 meters and a lower velocity (386 m/s mudstone) to the bottom of the borehole at 36.2 meters. The higher velocities at Anderson Dam (543 m/s), Calaveras Reservoir (728 m/s), Callens Ranch (1098 m/s), and Sunol Fire Station (934 m/s) are the result of decreased amounts of sand, increased gravel and cementation. The increase in texture (grain size) has been correlated with increasing S-wave velocity (e.g. Fumal, 1978). The average velocity to 35 meters (measurement at this depth in all seven boreholes) is 473 m/s, 501

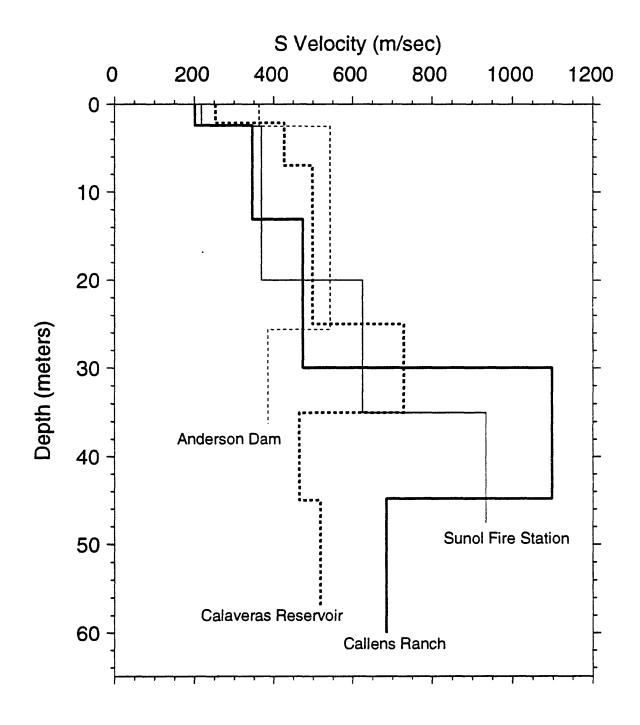


Figure 3. S-wave velocity models superimposed for comparison. The four sites shown here have higher average velocities in the upper sections of the borehole than those of Figure 4. Probably due to increased gravel content in the upper sections of the borehole.

m/s, 419 m/s, and 419 m/s for Anderson Dam, Calaveras Reservoir, Callens Ranch, and Sunol Fire Station, respectively.

Figure 4 summarizes the S-wave velocities at Hollister Airport, Webb Ranch, and Williams Ranch. The lithology of this group, in general, has less gravel content in the layering and therefore have lower average velocities than those of Figure 3. The average velocity to 35 meters is 223 m/s, 323 m/s, and 327 m/s for Hollister Airport, Webb Ranch, and Williams Ranch, respectively.

#### P-wave velocities

Figures 5 and 6 summarize the P-wave velocities at the seven sites of this report. There is a poorer correlation between P-wave velocity and lithology than between S-wave velocity and lithology because P-wave velocity is strongly affected by degree of saturation. The saturation level (water table) in unconsolidated sediments is sometimes indicated by an increase in P-wave velocity to near 1500 m/s. This is not always true as trapped gas (e.g. the presence of air, methane from decaying organic matter) can reduce the P-wave velocity below 1500 m/s even when the formation is saturated (Brandt, 1960).

#### APPENDIX

The appendix lists the detailed results, organized alphabetically by borehole. Figures and tables for each site are arranged in the following order:

- 1. location map
- 2. geologic log
- 3. record sections
- 4. time-depth graph
- 5. velocity profiles
- 6. velocity tables

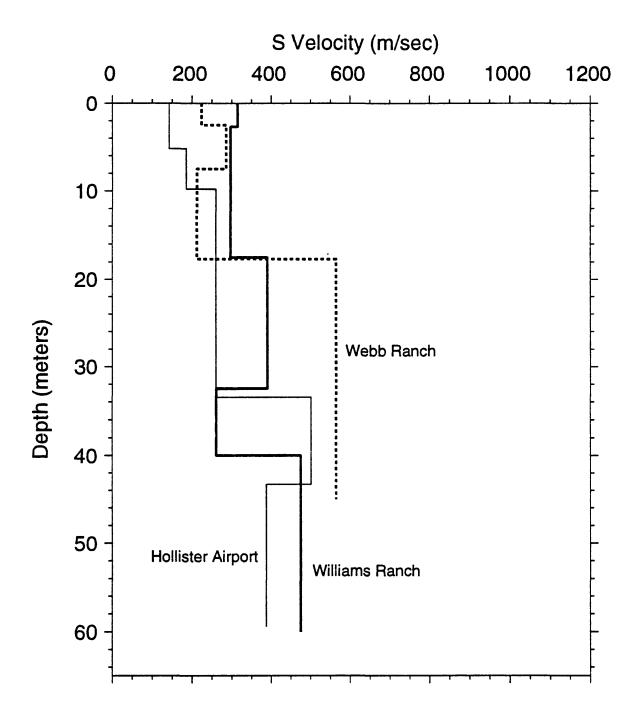


Figure 4. S-wave velocity models superimposed for comparison. In general, these three sites do not have as much gravel as those of Figure 3 and as a result have lower S-wave velocities in the uppers sections of the borehole.

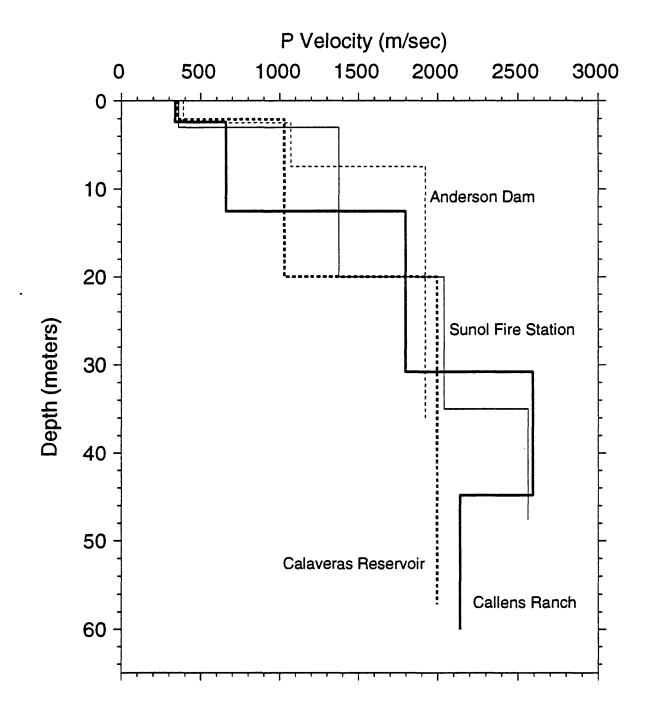


Figure 5. P-wave velocity models superimposed for comparison.

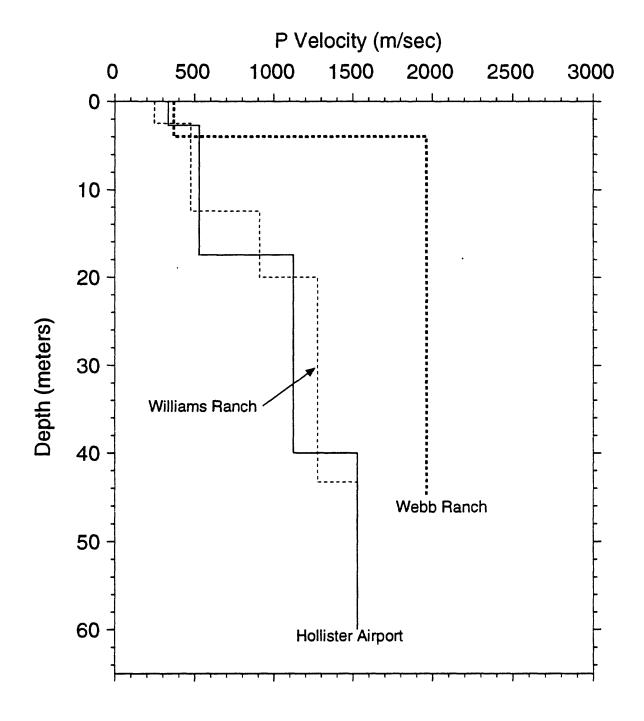


Figure 6. P -wave velocity models superimposed for comparison.

#### ACKNOWLEDGMENTS

We thank Mr. Robert Westerlund of the USGS for building the electrically actuated clamp for the borehole geophone and Dr. Hsi-Ping Liu of the USGS for designing the shear-wave generator. In addition, we were assisted in the field by Mr. Michael Carter, Miss Aina Fox, and Mr. Allen Foss of the USGS. We thank the following landowners for permission to drill on their land: Mrs. Thomas at Anderson Dam; Mr. Callens at Callens Ranch; Mrs. Williams at Williams Ranch and Mrs. Carpenter at Webb Ranch. We also thank Mr. Donald Jones of Quantic Industries Inc. at Calaveras Reservoir; Mr. Allen Ritter of Hollister Airport and Captain Carl Stanley of Sunol Forest Fire Station.

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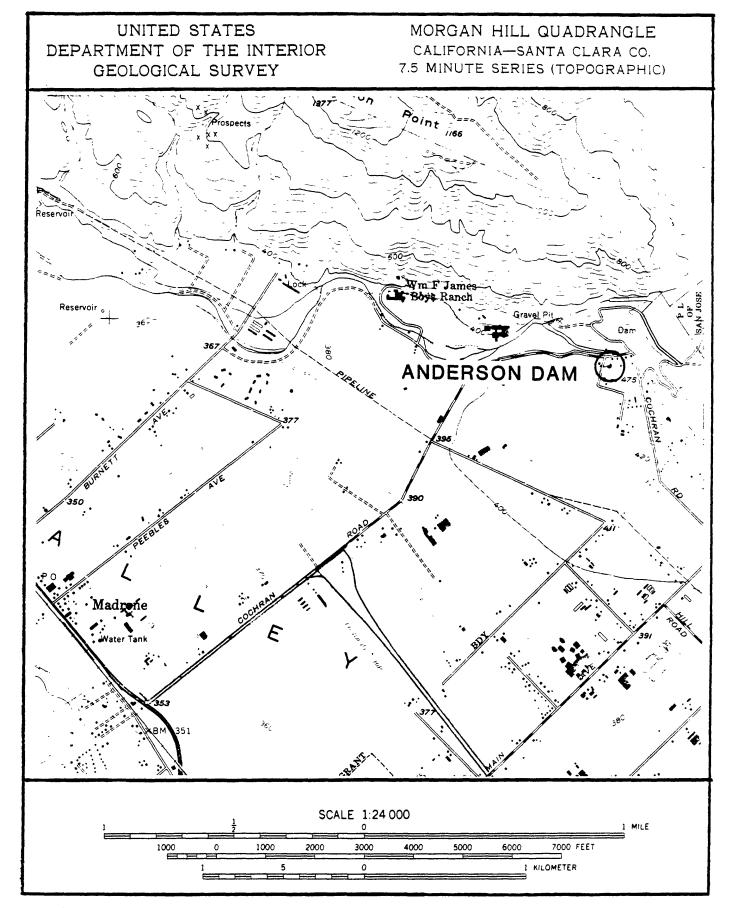


Figure 7. Site location map for the borehole at Anderson Dam (downstream) The borehole at Anderson Dam is located approximately 30 meters from the strong-motion recorder.

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

<u>cm</u>	<u>in</u>	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

#### Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight

discoloration

Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough dis-

coloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original

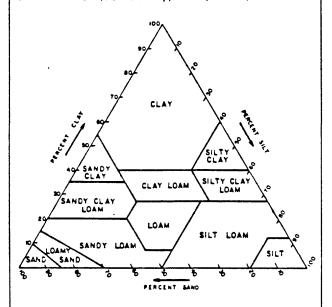
structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Figure 8. Explanation of geologic logs.

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

#### Types of samples

SP - Standard Penetration 1 + 3/8 in in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

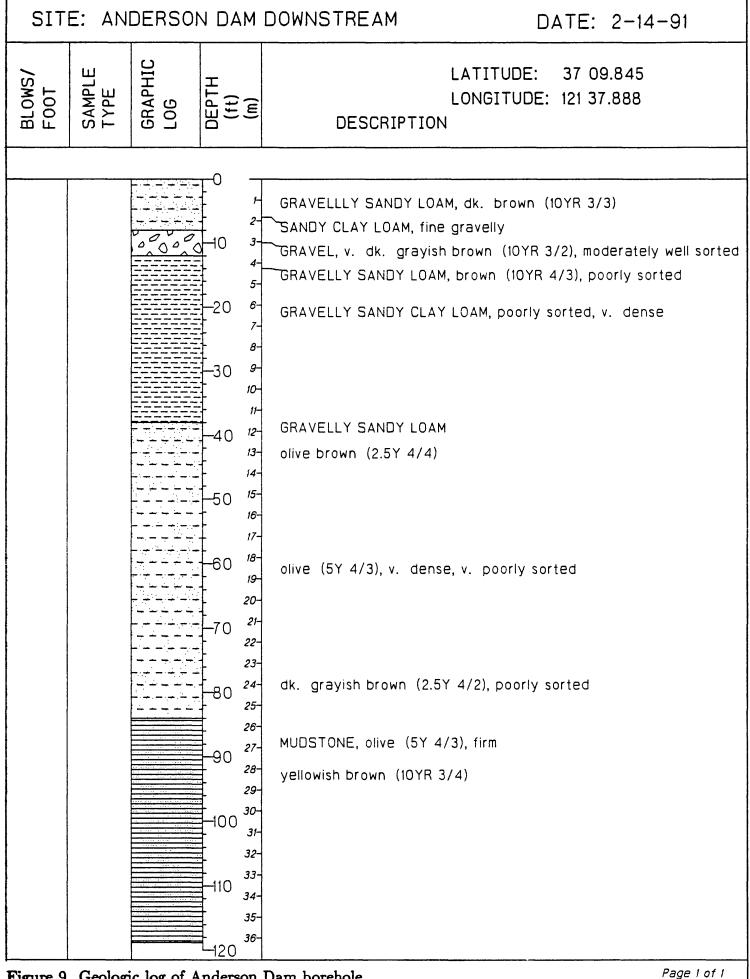


Figure 9. Geologic log of Anderson Dam borehole.

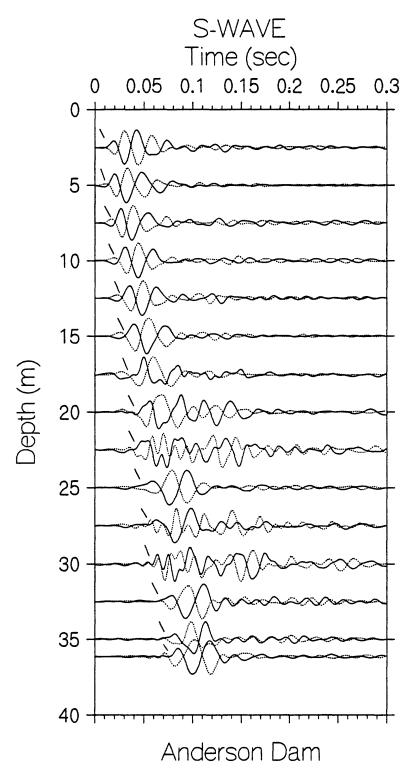


Figure 10. Record section of S-waves from impacts in opposite horizontal directions superimposed for indentification of S-wave onset. Approximate S-wave picks are shown by the accent marks.

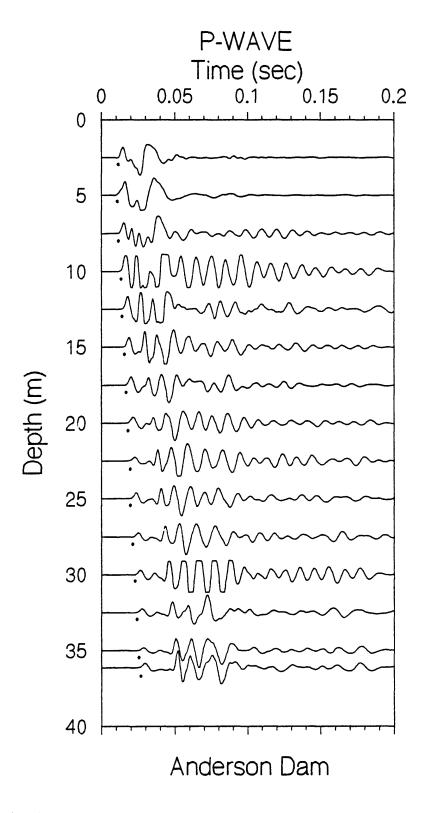


Figure 11. Vertical component record section. P-wave arrivals are shown by the solid circles.

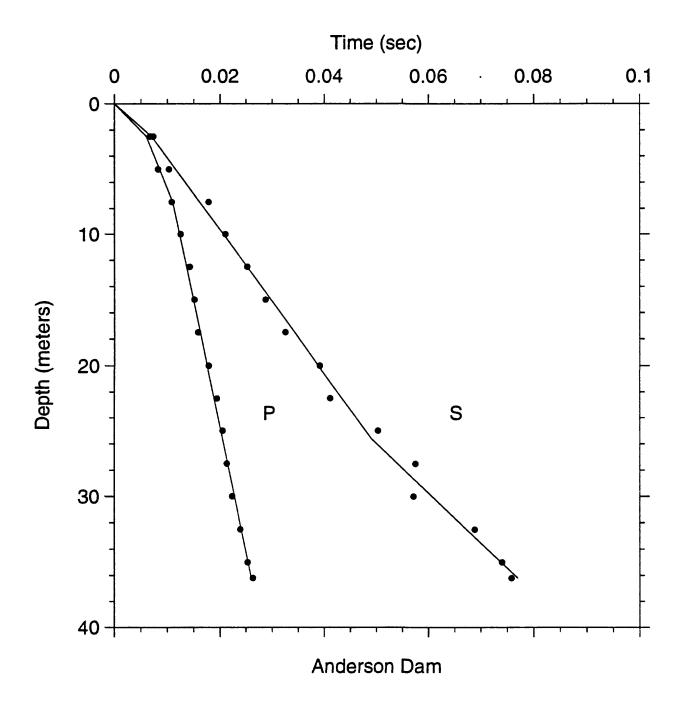


Figure 12. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

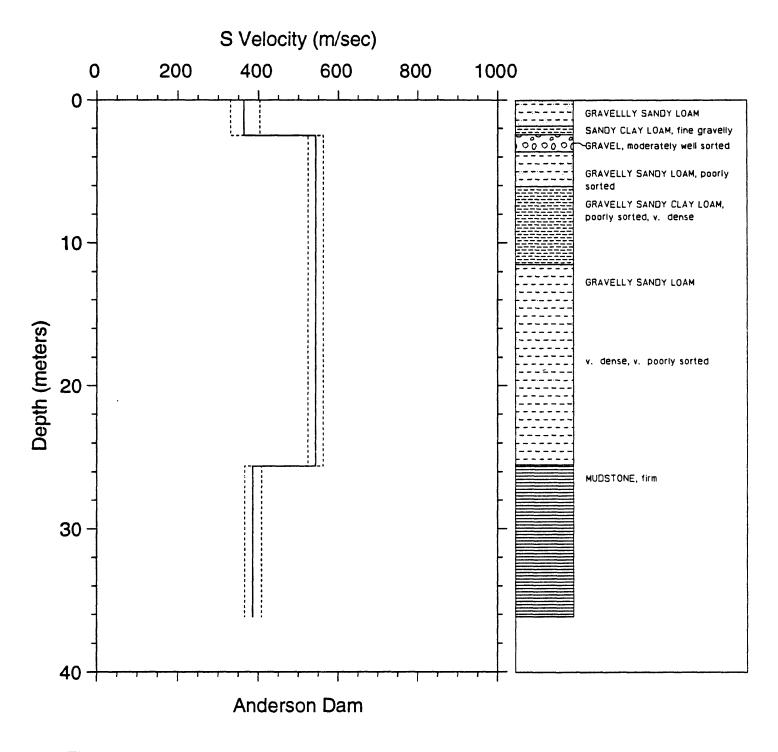


Figure 13. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

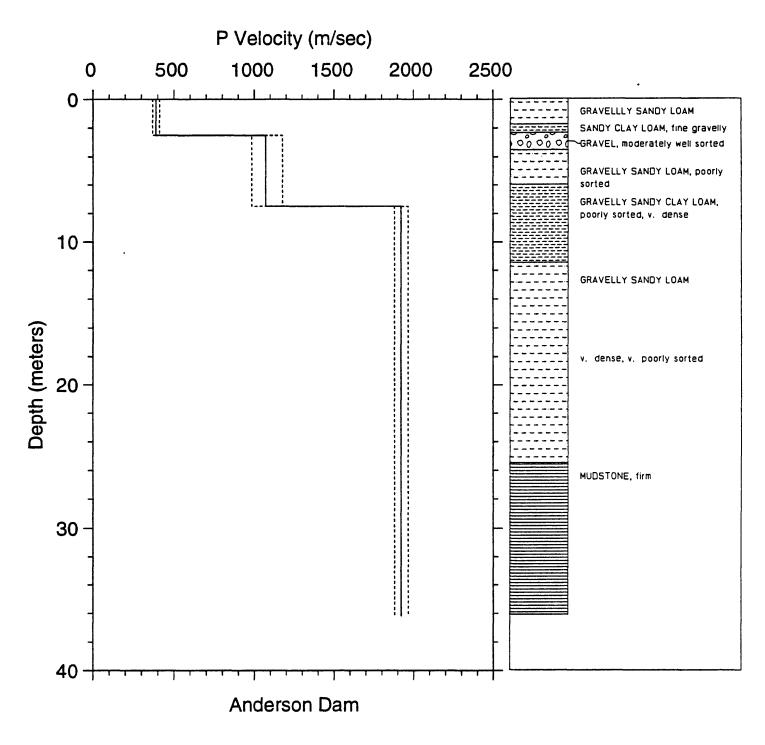


Figure 14. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

Page 1 of 1

TABLE 1. S-wave arrival times and velocity summaries for Anderson Dam (downstream).

vu(ft/s) 1321 1321 1843 1338
vl(ft/s) 1083 1083 1721 1199
(ft/s) 1190 1190 1780 1265
√u(m/s) 403 403 562 408
v((m/s) 330 330 524 366
v(m/s) 363 363 363 386 386
ttb(s) .000 .007 .049 .077
dtb(ft) 0.0 8.2 84.0 118.8
dtb(m) .0 .2.5 .5.5 36.2
rsdl/sig 
2 2
t(sec) s 0073 0073 0178 0210 0225 0287 0325 0391 0411 0575 0573 0573
d(ft) 8.2 16.4 16.4 32.8 32.8 47.0 65.6 73.8 82.0 98.4 114.8 114.8
45.55 25.50 25.50 25.50 25.50 35.50 35.50 35.50

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters dtb(ft) = depth to bottom of layer in feet

ttb(s) = arrival time in seconds to bottom of layer

vl(m/s) = lower limit of velocity in meters per second 4v(m/s) = velocity in meters per second

vu(m/s) = upper limit of velocity in meters per secondv(ft/s) = velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second vl(ft/s) = lower limit of velocity in feet per second

Page 1 of 1

TABLE 2. P-wave arrival times and velocity summaries for Anderson Dam (downstream).

vu(ft/s) 1350 1350	3862	6449											
vl(ft/s) 1211 1211	3224	6171											
v(ft/s) 1277 1277	3515	6307											
vu(m/s) 412 412	1177	1966											
vl(m/s) 369 369	983	1881											
v(m/s) 389 389	1071	1922											
ttb(s) .000 .006	.01	.026											
dtb(ft) .0 8.2	24.6	118.8											
dtb(m) .0 2.5	7.5	36.2											
rsdt/sig .3	۲.	Ξ.	'n	-	'n.	۲.	₹.	ĸ.	2		2		ĸ.
D	_	-		_	-	-	-	-	-	_	<del>-</del>	_	-
t(sec) 8.0067	.0108	.0125	.0142	.0151	.0158	.0178	.0194	.0205	.0213	.0223	.0239	.0253	.0263
d(ft) 8.2 16.4	54.6	32.8	41.0	49.5	57.4	9.59	73.8	82.0	90.5	98.4	106.6	114.8	118.8
d(m)	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0	27.5	30.0	32.5	35.0	36.5

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from

hammer blows differing in direction by 180°) sig = sigma, stardard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

ttb(s) = arrival time in seconds to bottom of layer <math>v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second <math>vu(m/s) = upper limit of velocity in meters per second <math>v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second
vu(ft/s) = upper limit of velocity in feet per second
\* see text for explanation of velocity limits

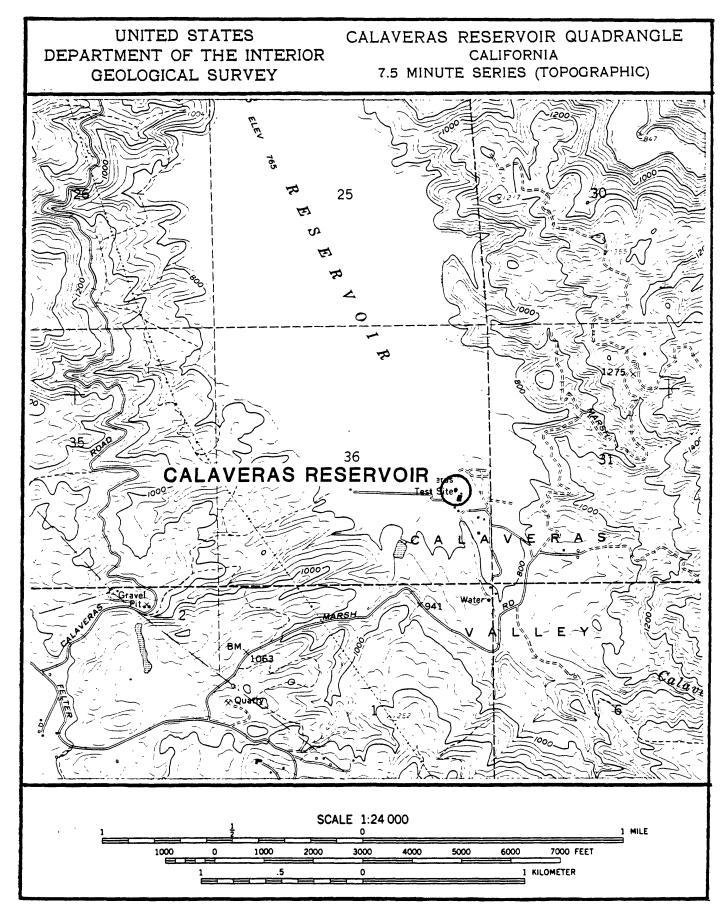


Figure 15. Site location map for Calaveras Reservoir borehole.

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

<u>cm</u>	<u>ic</u>	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

#### Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight

discoloration

Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough dis-

coloration

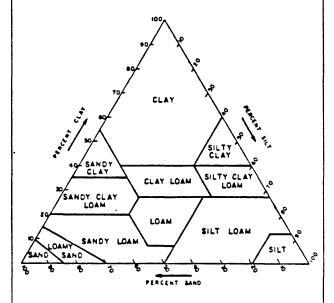
Deep: extensive decomposition of minerals and complete disintegration of rock but original

structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

#### Types of samples

- SP Standard Penetration 1 + 3/8 in in ID sampler)
- S Thin-wall push sampler
- O Osterberg fixed-piston sampler
- P Pitcher Barrel sampler
- CH California Penetration (2 in ID sampler)
- DC Diamond Core

Figure 16. Explanation of geologic log.

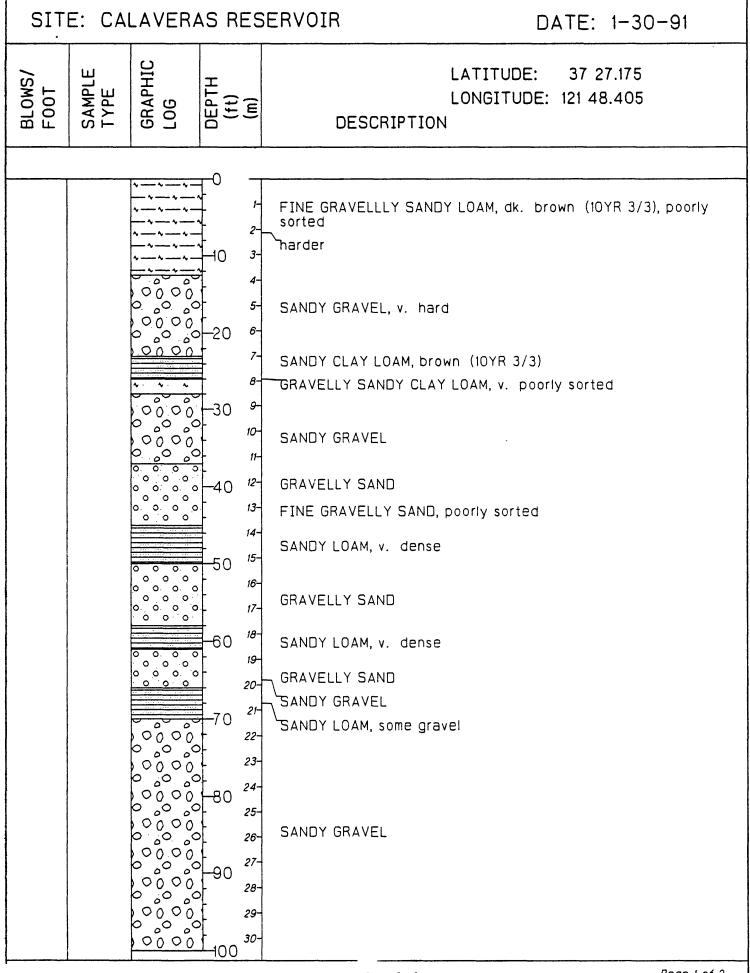


Figure 17. Geologic log of Calaveras Reservoir borehole.

Page 1 of 2

SIT	E: CA	LAVERA	AS RES	SERVOIR DATE: 1-30-91
BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	LATITUDE: 37 27.175 LONGITUDE: 121 48.405 DESCRIPTION
		ار الحراد ا	7 100 T	
			31- 32- 33- -110 34- 35-	SANDY GRAVEL
		0 0	36- -120 37- 38-	SANDY CLAY LOAM, olive (5Y 4/3), v. dense
		V > V > V	39- -130 40-	GRAVELLLY SANDY LOAM, poorly sorted
			41- 42- 140 13	SANDY CLAY LOAM, some gravel, (5G 2/1), dk. greenish gray
			44-	rocky
		0000	+ 407	SANDY GRAVEL, olive brown (2.5Y 4/4) to dk. grayish brown (2.5Y 4/2), poorly sorted
			160 49 50-	SANDY LOAM, olive (5Y 4/3)
		<pre></pre>	170 <i>52</i> - 53- 54-	
		< ^ V < ^ V <	-180 <i>55-</i>	GRAVELLY SANDY LOAM  v. hard
		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	57- 190 58-	
			- 59- 60- -200	
Figur	e 17. (C	ontinued)		Page 2 of 2

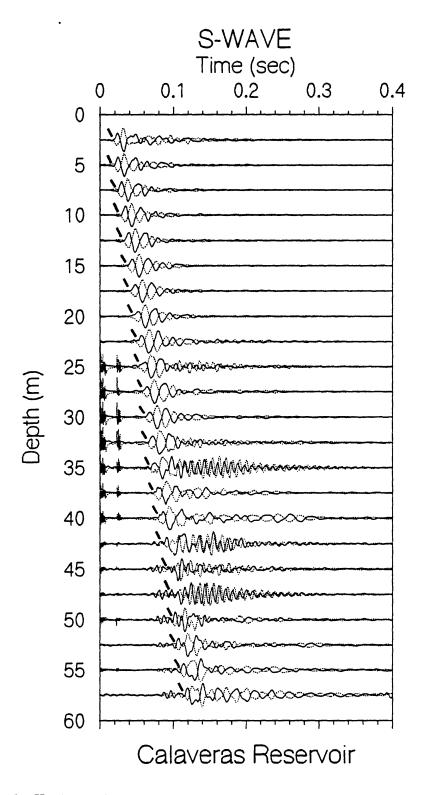


Figure 18. Horizontal-component record section (from horizontal impacts in opposite directions) superimposed for identification of S-wave arrivals. Approximate S-wave picks are shown by the accent marks.

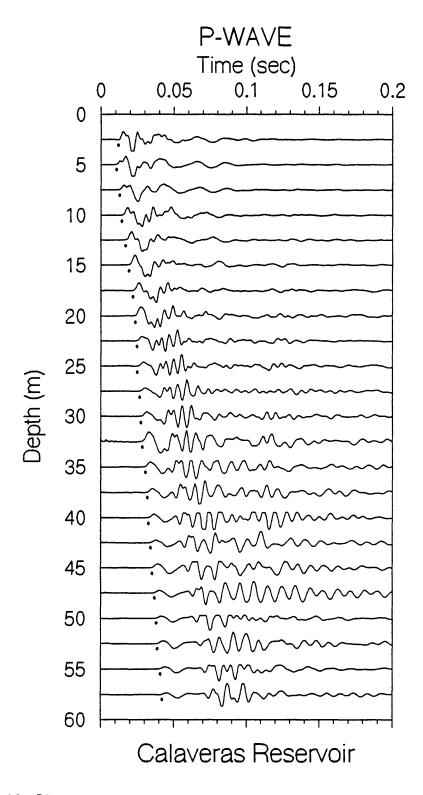


Figure 19. Vertical-component record section. Approximate P-wave picks are shown by the solid circles.

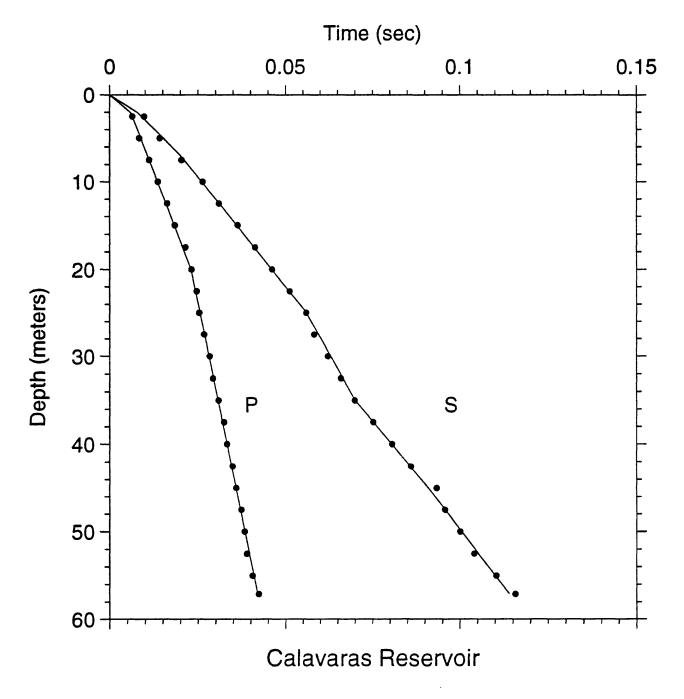


Figure 20. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

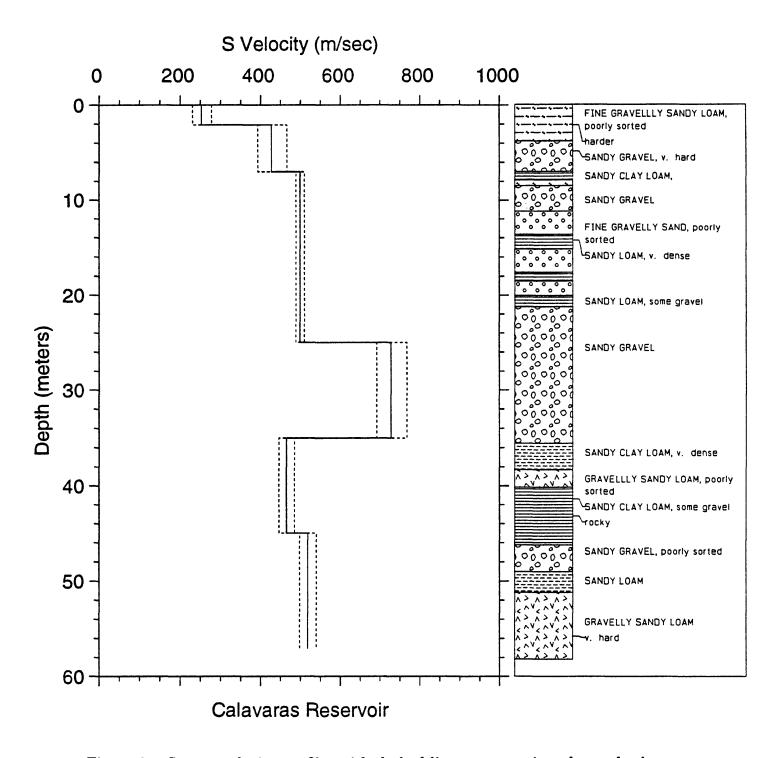


Figure 21. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

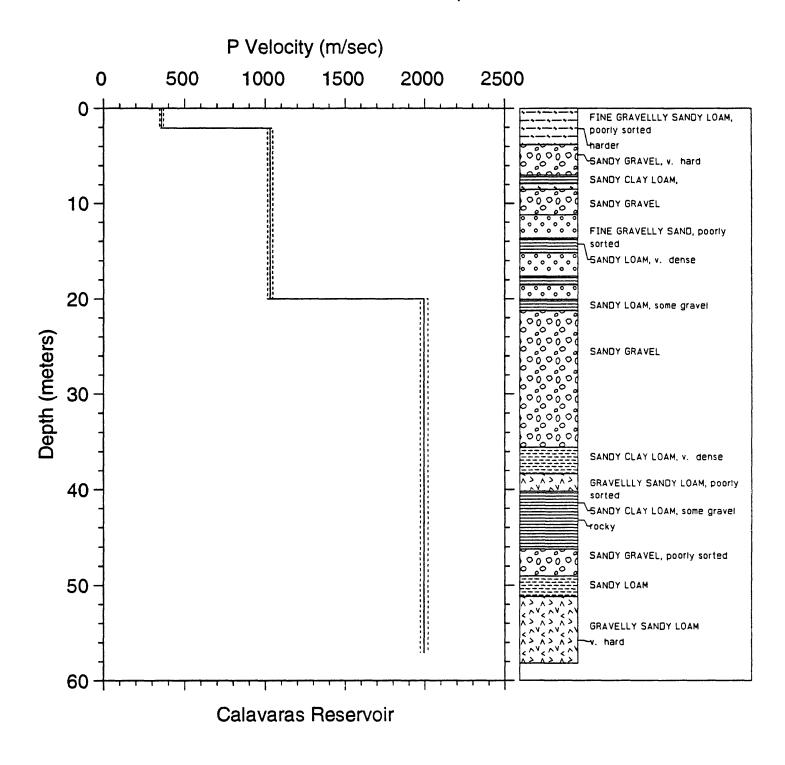


Figure 22. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

TABLE 3. S-wave arrival times and velocity summaries for Calaveras Reservoir.

m) dtb(ft) ttb(s) v(m/s) v((m/s) vu(ff/s) v(ff/s) vu(ff/s) vu(ff/s	Explanation:	d(m) = depth in meters	$d(\mathbf{ft}) = depth$ in feet	t(sec) = arrival time in seconds (S-wave arrival times are	the average of picks from traces obtained from hammer blows differing in direction by 180°)	sig = sigma, standard deviation normalized to the	standard deviation of best picks rsdl/sig = least-squares residual divided by sigma	dtb(m) = depth to bottom of layer in meters	dtb(ft) = depth to bottom of layer in feet ttb(s) = arrival time in seconds to bottom of layer	) = velocity in meters per second	v(m/s) = lower limit of velocity in meters per second * vu(m/s) = upper limit of velocity in meters per second	v(ft/s) = velocity in feet per second	vl(ft/s) = lower limit of velocity in feet per second $vu(ft/s) = upper limit of velocity in feet per second$	* see text for explanation of velocity limits
dtb(m) - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -														
Day   8   8   8   8   8   8   8   8   8	-1.5	<u> </u>												

d(ft) t(sec) s 8.2 .0097 16.4 .0141 24.6 .0203 32.8 .0263 41.0 .0369 49.2 .0363 57.4 .0413 65.6 .0461 73.8 .0512 80.2 .0559 90.2 .0559 90.2 .0559 114.8 .0659 114.8 .0659 1135.0 .0559 1147.6 .0934 1155.8 .0957 1164.0 .1103 187.2 .1103

TABLE 4. P-wave arrival times and velocity summaries for Calaveras Reservoir.

v(m/s) vl(m/s) vu(ft/s) vl(ft/s) vu(ft/s) 357 346 370 1173 1134 1214 357 346 370 1173 1134 1214 1030 1014 1046 3380 3328 3433 1995 1971 2020 6546 6465 6629	Explanation:  d(m) = depth in meters d(ft) = depth in feet  t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)  sig = sigma, standard deviation normalized to the standard deviation of best picks  rsdl/sig = least-squares residual divided by sigma dtb(m) = depth to bottom of layer in meters dtb(ft) = arrival time in seconds to bottom of layer v(m/s) = velocity in meters per second v(m/s) = lower limit of velocity in meters per second v(ft/s) = velocity in feet per second v(ft/s) = lower limit of velocity in feet per second v(ft/s) = lower limit of velocity in feet per second vu(ft/s) = lower limit of velocity in feet per second vu(ft/s) = upper limit of velocity in feet per second
(tb(s) .000 .003 .023	면 *
dtb(m) dtb(ft) ttb(s) 2.0 0.0 2.1 6.9 .003 20.0 65.6 .023 57.1 187.3 .042	
dtb(m) 2.0 2.1 20.0 57.1	
28d 78d 78d 78d 78d 78d 78d 78d 7	
t (sec) .0064 .0111 .01116 .0132 .0253 .0253 .0253 .0253 .0253 .0253 .0253 .0253 .0253 .0253	. 0383 . 0425 . 0423
	o'u'4w'

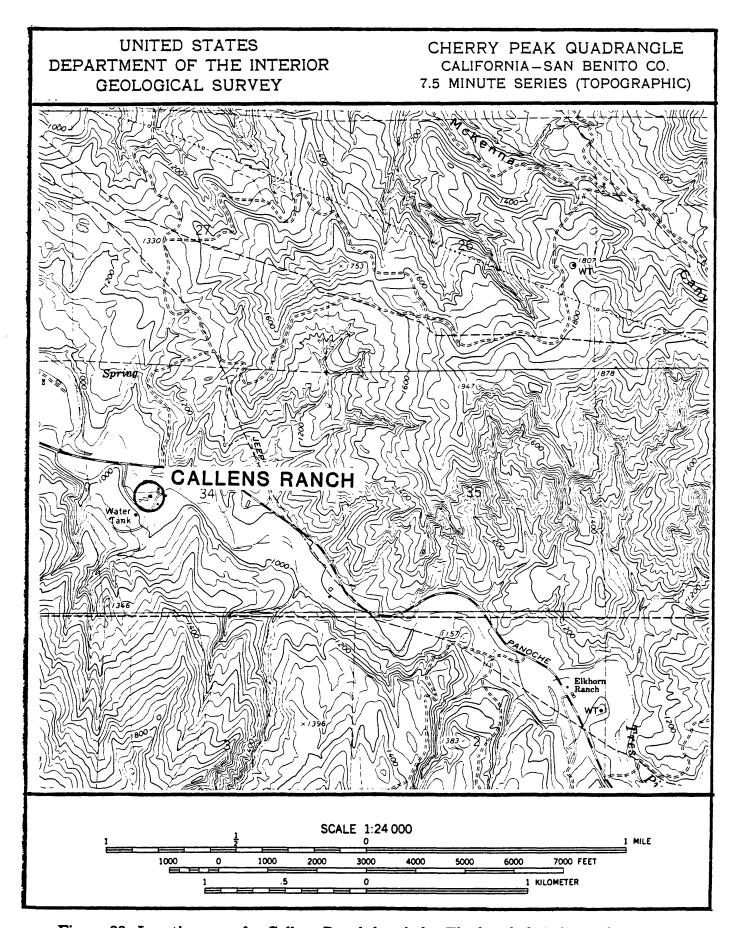


Figure 23. Location map for Callens Ranch borehole. The borehole is located approximatelly 20 meters from the strong-motion accelerograph.

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

<u>cm</u>	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

# Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight

discoloration

Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough dis-

coloration

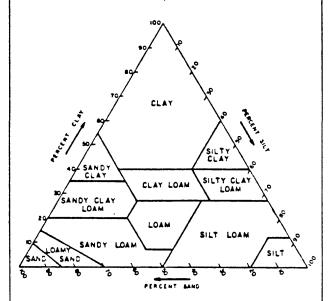
Deep: extensive decomposition of minerals and complete disintegration of rock but original

structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

# Types of samples

SP - Standard Penetration 1 + 3/8 in in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 24. Explanation of geologic log.

SIT	E: CA	LLENS	RANCH	DATE: 3-19-91
BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	LATITUDE: 36 40.390 LONGITUDE: 121 11.725 DESCRIPTION
			•	
			P 2-	SANDY CLAY LOAM, dk. grayish brown (2.5Y 4/2)
			10 3- 4-	GRAVELLY SANDY LOAM, poorly sorted
			5- 20 6-	LOAM-SAND, sand is v. fine to v. coarse size
0			7- 8-	SAND, with thin lenses of gravel
			-30 9- 10-	GRAVELLY v. coarse SAND, grayish brown
			40 12-	SANDY GRAVEL  GRAVEL, coarse
			14-	SILTY CLAY, olive (5Y 5/3)  olive brown (2.5Y 4/4)
			50 <sup>/3</sup> 	SILTY CLAY LOAM to SILT LOAM, v. dk. greenish gray (5GY 3/1)
			60 <sup>18</sup> -	stiff SILTY CLAY, v. dk. greenish gray (5GY 3/1), v. stiff
			20- -70	
			22-	
			80 <sup>24</sup> -	
			26- 27- 90 28-	
			29-	
Ti:- C:			<del>-</del> 100	Ranch borehole. Page 1 of 2

SIT	E: CA	LLENS	RANCH	DATE: 3-19	9-91
BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	LATITUDE: 36 40.390 LONGITUDE: 121 11.725 DESCRIPTION	
			-100 -		
			31- 32- - - - - - - - - - - - - - - - - -		to
			1 35-	SANDY GRAVEL, cemented	
		0000	120	Total tell beds of oldy	
		0000	7 37-	SILTY CLAY SANDY GRAVEL, cemented	
			1	SAND TONAVEE, COMERCE	
		0000	1 100		
		0000	42-		
		0000	140 43		
		0000	44-		
			150 <sub>46-</sub>	MUDSTONE, firm (texture is silty clay)	
			47-		
			48- 160 <sub>49-</sub>		
			50-		
			51- 170 52-	SILTY CLAY, dk. greenish gray (5BG 4/1), softer	
			53-		
			54-		
			180 55		
			56- 57- -190 58-		
			59- 60-	SILTY CLAY LOAM, dk. gray (5Y 4/1)	
			1_200		
Figure 2	5. (Con	tinued).		40	Page 2 of 2

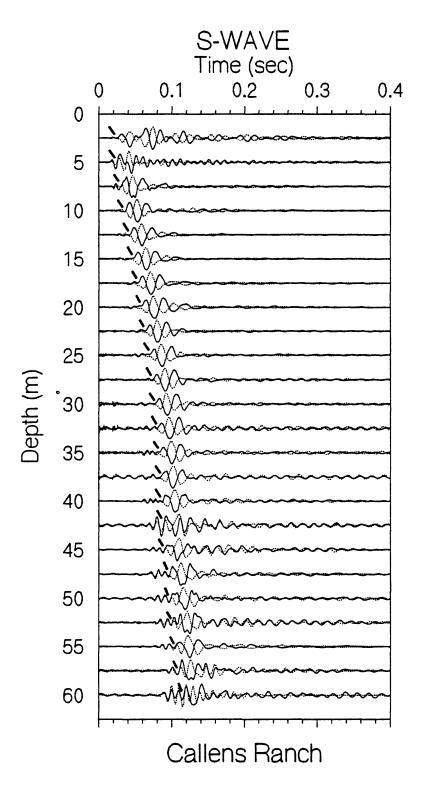


Figure 26. Horizontal-component record section (from horizontal impacts in opposite directions) superimposed for identification of S-wave onset. Approximate S-wave picks are indicated by the accent marks.

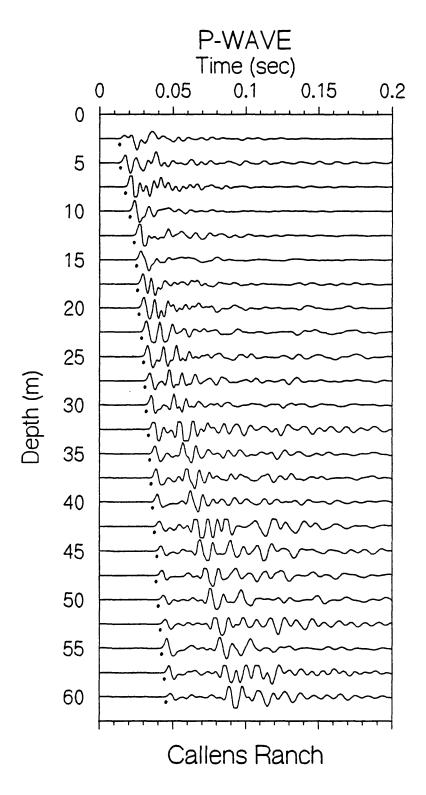


Figure 27. P-wave record section. Approximate P-wave picks are shown by the dots.

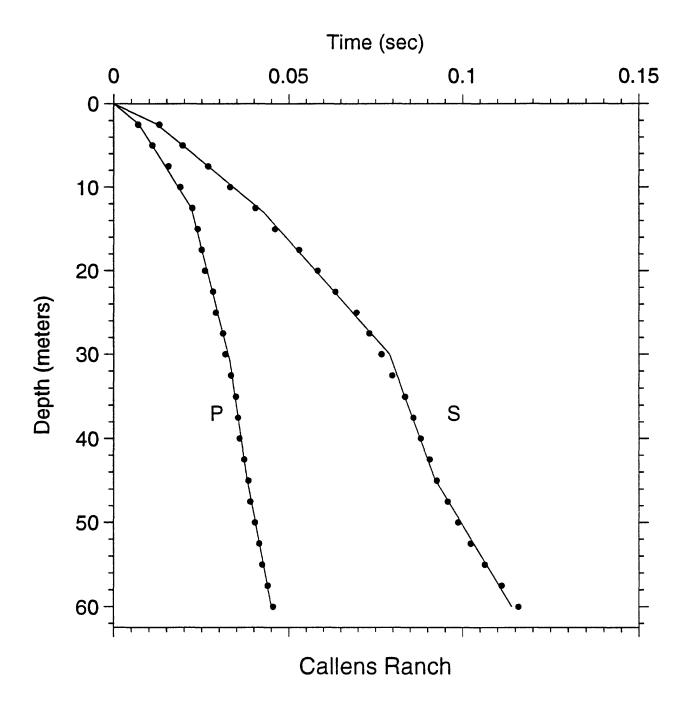


Figure 28. Time-depth graph of P-wave and S-wave picks. Line segments show the hing-least-squares fit to the data.

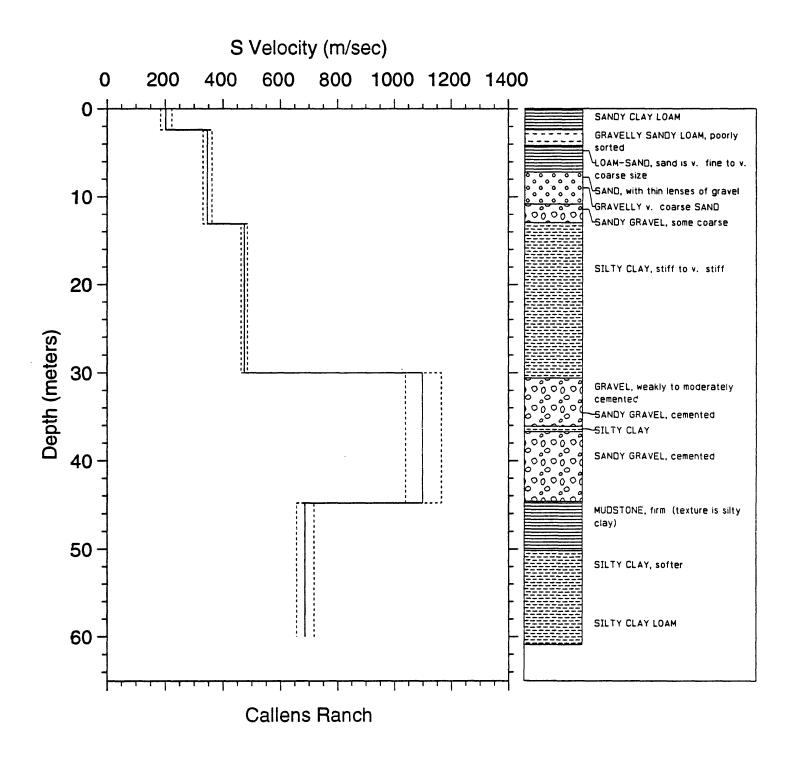


Figure 29. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

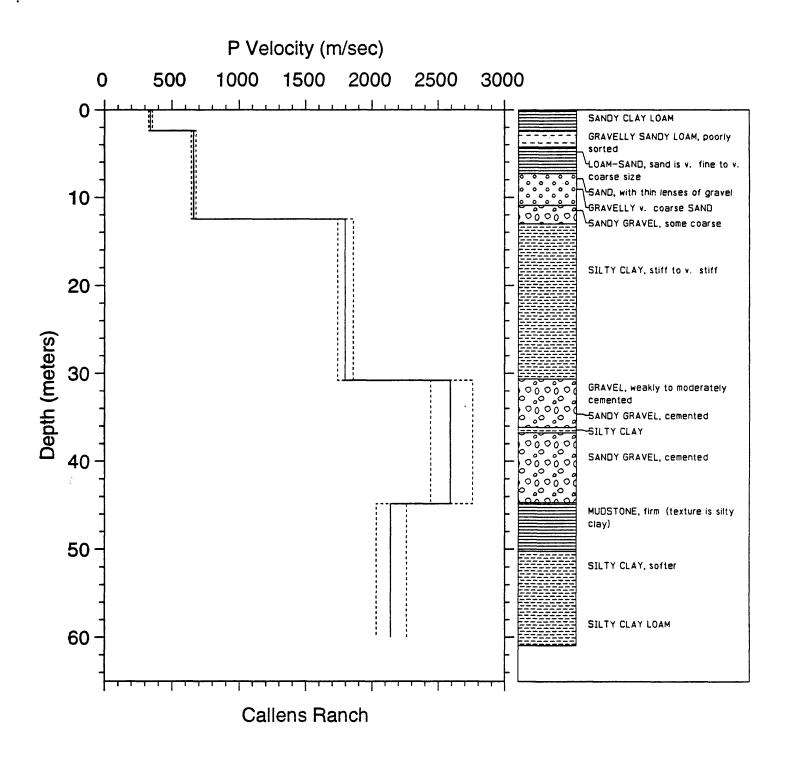


Figure 30. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

TABLE 5. S-wave arrival times and velocity summaries for Callens Ranch site.

dtb(m) dtb(ft) ttb(s) v(m/s) vu(m/s) vu(ft/s) vu	Explanation:  d(m) = depth in meters d(ft) = depth in feet t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°) sig = sigma, standard deviation normalized to the standard deviation of best picks rsdl/sig = least-squares residual divided by sigma dtb(m) = depth to bottom of layer in meters dtb(ft) = depth to bottom of layer in feet ttb(s) = arrival time in seconds to bottom of layer v(m/s) = velocity in meters per second v(ft/s) = lower limit of velocity in meters per second v(ft/s) = lower limit of velocity in feet per second v(ft/s) = upper limit of velocity in feet per second v(ft/s) = upper limit of velocity in feet per second vu(ft/s) = upper limit of velocity in feet per second vu(ft/s) = upper limit of velocity limits
1 Psd (	2-2-8 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.
To a second seco	N

455.55 6.55

TABLE 6. P-wave arrival times and velocity summaries for Callens Ranch site.

	<pre>vl(ft/s) = lower limit of velocity in feet per second vu(ft/s) = upper limit of velocity in feet per second * see text for explanation of velocity limits</pre>
00000000000000000000000000000000000000	

t(sec) .0069 .0109 .0109 .0109 .0282 .0282 .0282 .0284 .0317 .0317 .0334 .0358 .0378 .0378 .0378 .0378 .0378 .0378

dft) 8.2.4.16.24.1

45.0 45.0 45.0 45.0 45.0 45.0 60.0 

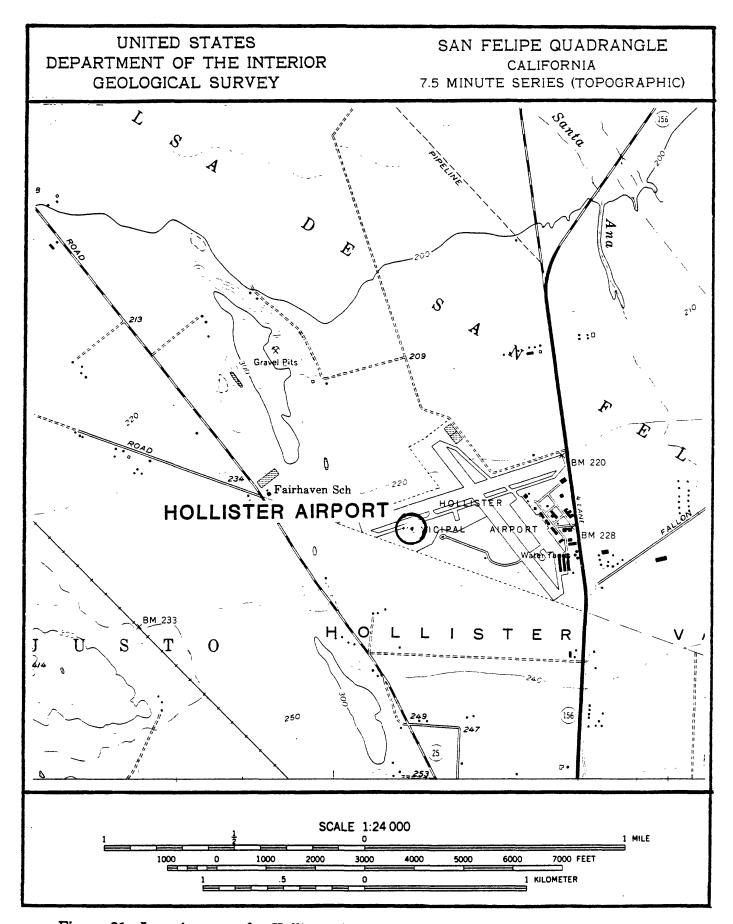


Figure 31. Location map for Hollister Airport borehole. The strong-motion accelerograph is located within 20 meters of the borehole.

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

<u>cm</u>	<u>in</u>	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	ciose
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

# Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

discoloration

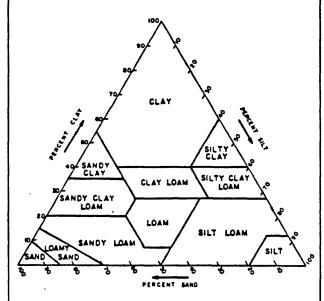
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

<u>blows/ft.</u>	relative density	<u>blows/ft.</u>	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).

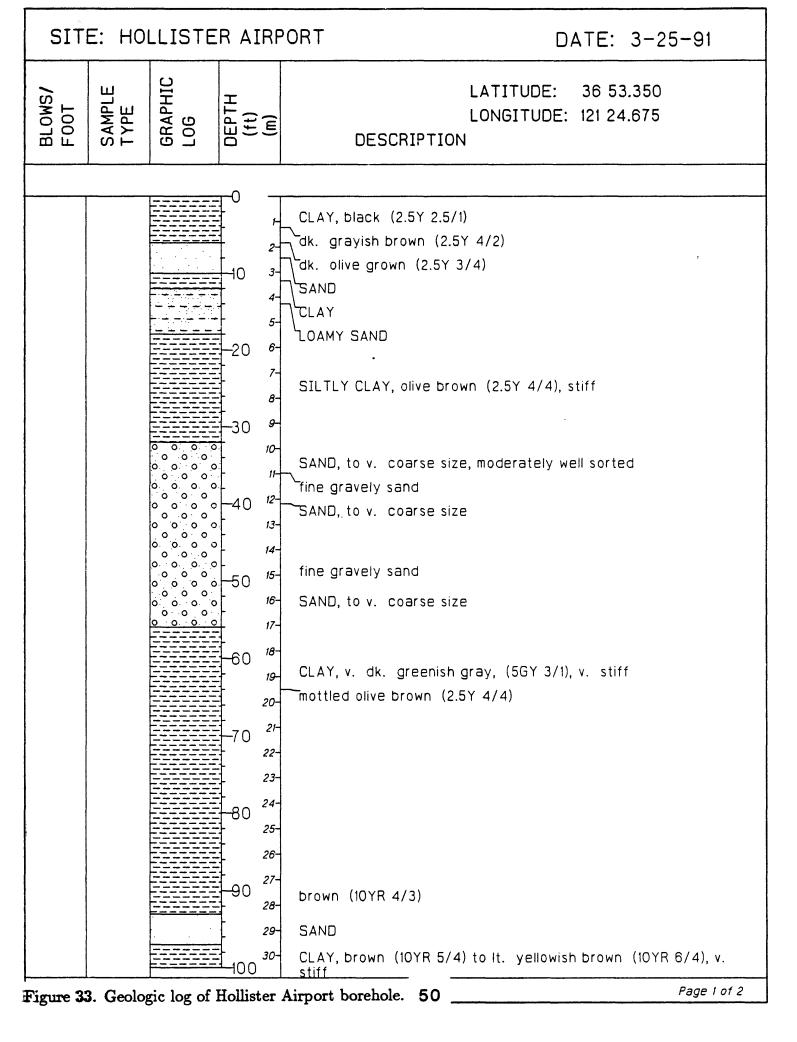


Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

# Types of samples

- SP Standard Penetration 1+3/8 in in ID sampler)
- S Thin-wall push sampler
- O Osterberg fixed-piston sampler
- P Pitcher Barrel sampler
- CH California Penetration (2 in ID sampler)
- DC Diamond Core

Figure 32. Explanation of geologic log.



SIT	E: HO	LLISTE	R AIRF	ORT DATE: 3-25-91
BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	LATITUDE: 36 53.350 LONGITUDE: 121 24.675 DESCRIPTION
			40.0	
	ng gang gang ang ang ang ang ang ang ang		31-	CLAY, brown (10YR 5/4) to It. yellowish brown (10YR 6/4), v. stiff
			33- 110 34-	SANDY CLAY, It. yellowish brown (10YR 6/4)
		0000	35-	GRAVELLY SAND, v. dense
			120 37-	CANDY CRAVEL hard
			38- - 39-	
			H30	
			42-	
		0 0 0 0		SILTY CLAY LOAM, grayish brown (2.5Y 5/2)
		0000	45- 150 46-	GRAVELLY SAND
			47-	SANDY CLAY LOAM, grayish brown (2.5Y 5/2)
		0 0 0	160 49	SANDY GRAVEL
		00.00	5 - 50-	SANDY CLAY LOAM
		0 0 0 0	5 <i>t</i> -	GRAVELLY SAND
		0000	-170 <i>52</i> -	SANDY GRAVEL
		0000	53-	GRAVELLLY SAND
			54-	SANDY CLAY LOAM, denser
			180 <i>55</i>	
			56- 57-	SILT LOAM, olive gray (5Y 4/2), denser
			190 <i>58</i> -	
		<del>5-,5-,</del> 5	59-	GRAVELLY SAND
		0000	200	
Figure	<b>33</b> (Co	ntinued).	***************************************	51Page 2 of 2

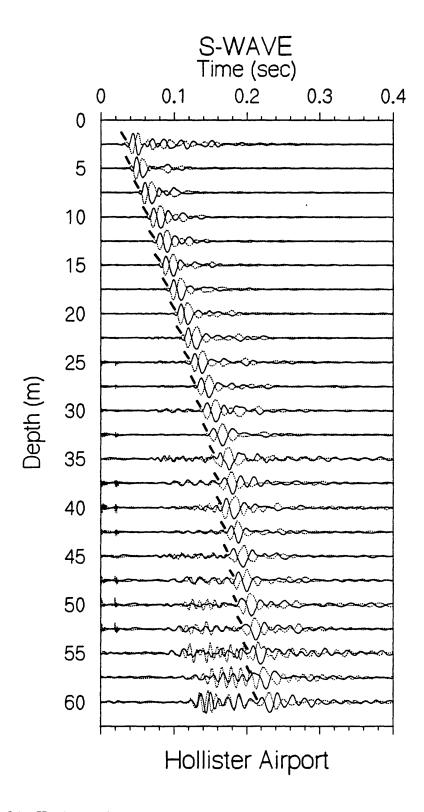


Figure 34. Horizontal-component record section (from horizontal impacts in opposite directions) superimposed for identification of S-wave onset. Approximate S-wave picks are indicated by the accent marks.

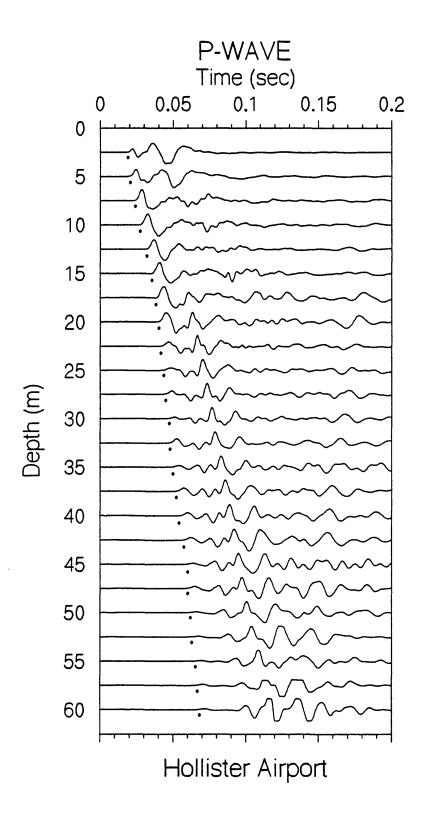


Figure 35. Vertical-component record section. Approximate P-wave picks are shown by the solid circles.

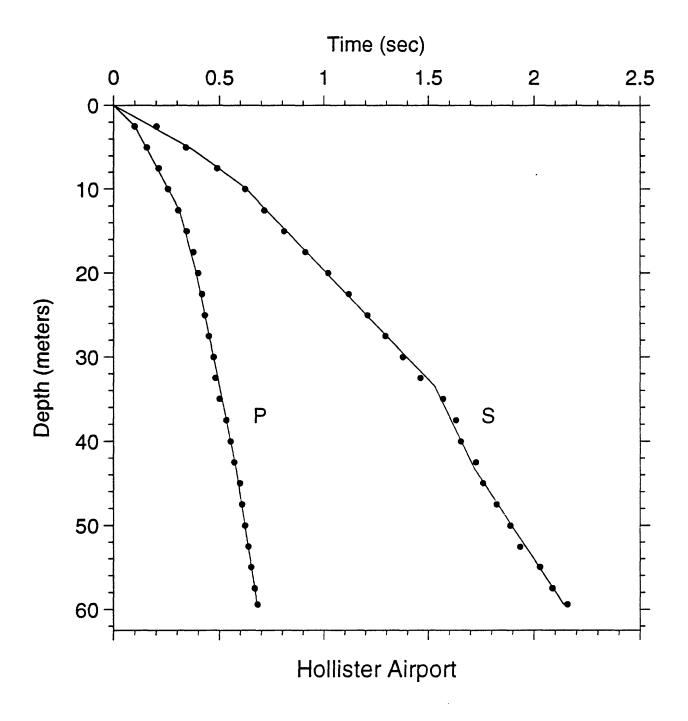


Figure 36. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

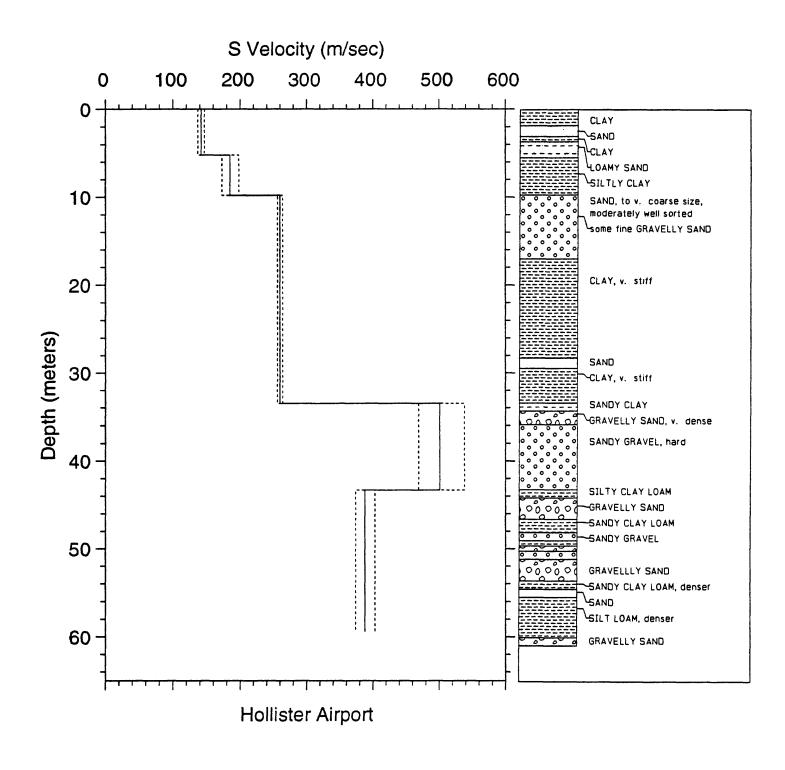


Figure 37. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

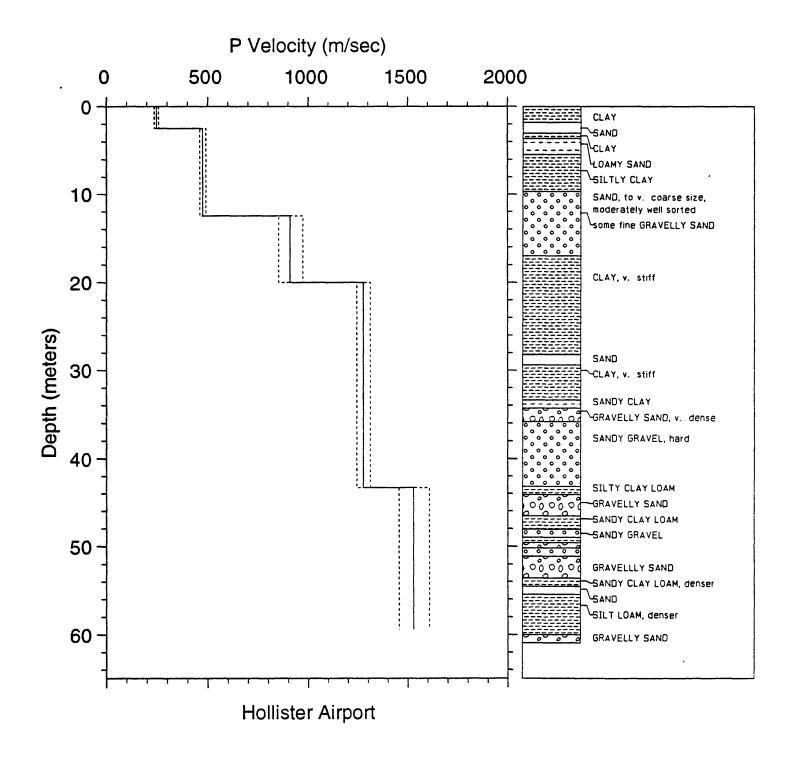


Figure 38. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

vu(ft/s) = upper limit of velocity in feet per second

\* see text for explanation of velocity limits

TABLE 7. S-wave arrival times and velocity summaries for Hollister Airport site.

dtb(m) dtb(ft) ttb(s) v(m/s) v((m/s) v(ft/s) vu(ft/s) vu(	Explanation:	d(m) = depth in meters	d(ft) = depth in feet	ÎI (	the average of picks from traces obtained from	hammer blows differing in direction by 180°)	sig = sigma, standard deviation normalized to the	rsdl/sig = least-squares residual divided by sigma	dtb(m) = depth to bottom of layer in meters	dtb(ft) = depth to bottom of layer in feet	ttb(s) = arrival time in seconds to bottom of layer	v(m/s) = velocity in meters per second	vl(m/s) = lower limit of velocity in meters per second *	vu(m/s) = upper limit of velocity in meters per second	v(ft/s) = velocity in feet per second	vi(ft/s) = lower limit of velocity in feet per second
<b>t</b>																
25.1	-2.6		1.9													
To a second seco	← •		-													
	. 1934	2087	.2157													
			_													

455.50 645.50

TABLE 8. P-wave arrival times and velocity summaries for Hollister Airport site.

dtb(m) dtb(ft) ttb(s) v(m/s) v(l(m/s) vu(ft/s) v	Explanation:		t(sec) = arrival time in seconds (S-wave arrival times are	the average of picks from traces obtained from hammer blows differing in direction by 180°)	sig = sigma, standard deviation normalized to the	standard deviation of best picks	redi/sig = least-squares residual divided by sigma	dtb(ft) = depth to bottom of layer in feet	ttb(s) = arrival time in seconds to bottom of layer	v(m/s) = velocity in meters per second	v(m/s) = lower limit of velocity in meters per second **	$vu(m/s) = upper mine or velocity in meters per second v(f_1/s) = velocity in feet per second$	v((t/s)) = lower limit of velocity in feet per second	vu(ft/s) = upper limit of velocity in feet per second	* see text for explanation of velocity limits
	٥.														
28 2 4 2 5 4 5 8 7 1 2 5 4 5 6 1 8 8 4 5 6 5 6 1 8 8 4 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	σ r	V 80 V													

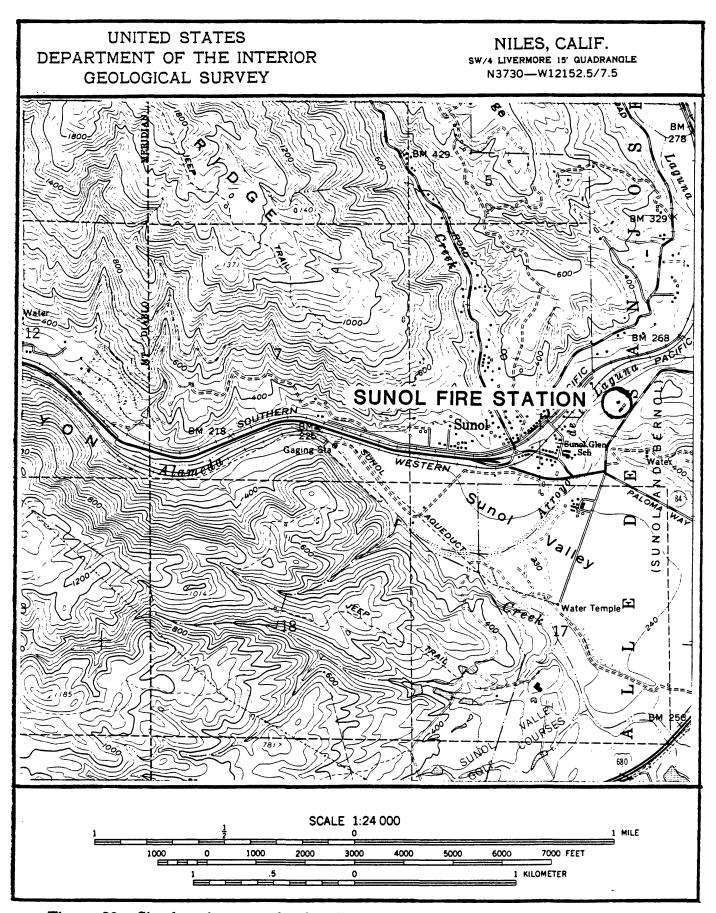


Figure 39. Site location map for Sunol Fire Station borehole. The strong-motion accelerograph is located approximately 30 meters from the borehole.

hard - hammer bounces off with solid sound .

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

<u>cm</u>	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

# Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

discoloration

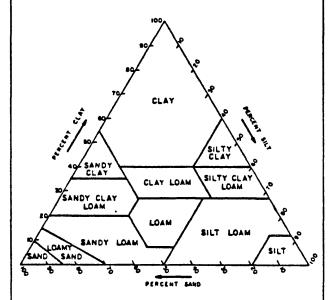
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough dis-

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

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- S Thin-wall push sampler
- O Osterberg fixed-piston sampler
- P Pitcher Barrel sampler
- CH California Penetration (2 in ID sampler)
- DC Diamond Core

Figure 40. Explanation of geologic logs.

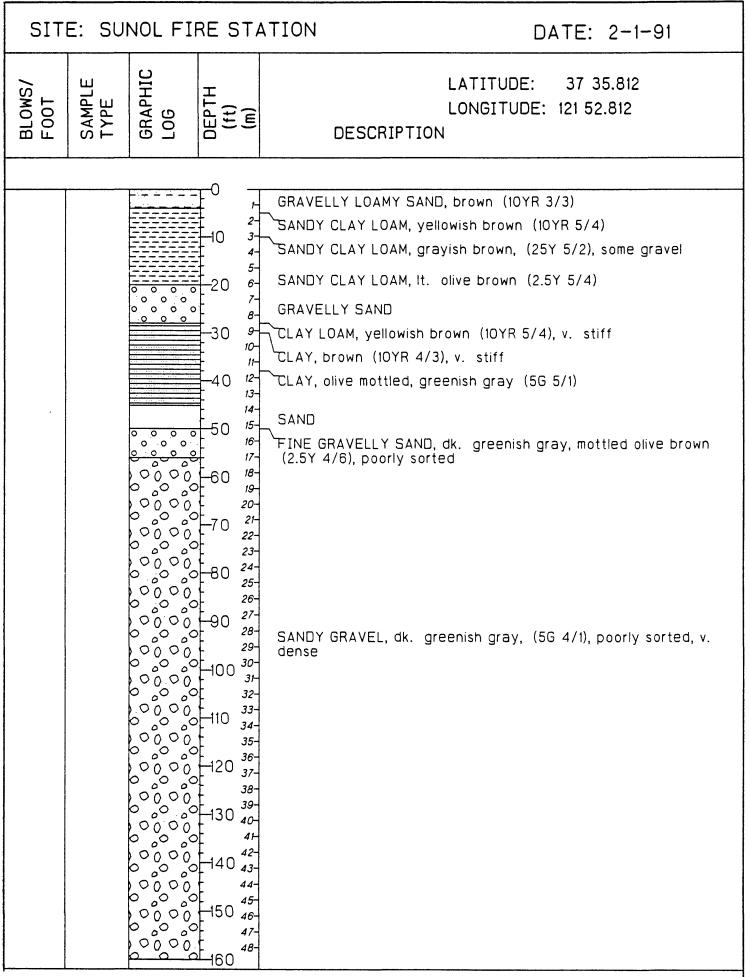


Figure 41. Geologic log of Sunol Fire Station borehole.

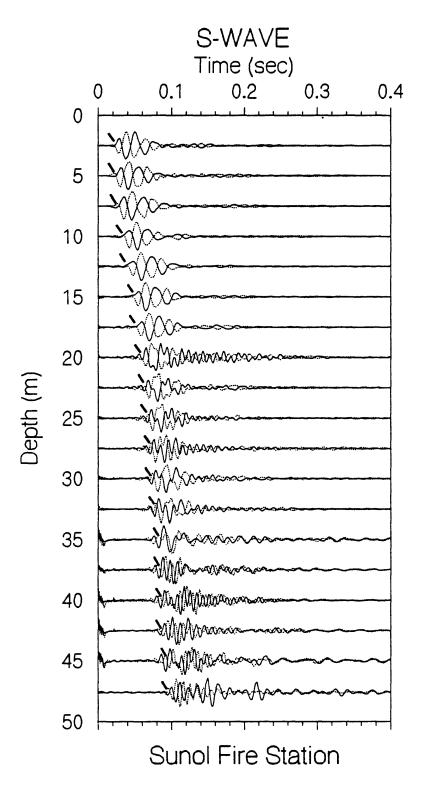


Figure 42. Horizontal-component record section (from horizontal impacts in opposite directions) superimposed for identification of S-wave onset. Approximate S-wave picks are indicated by the accent marks.

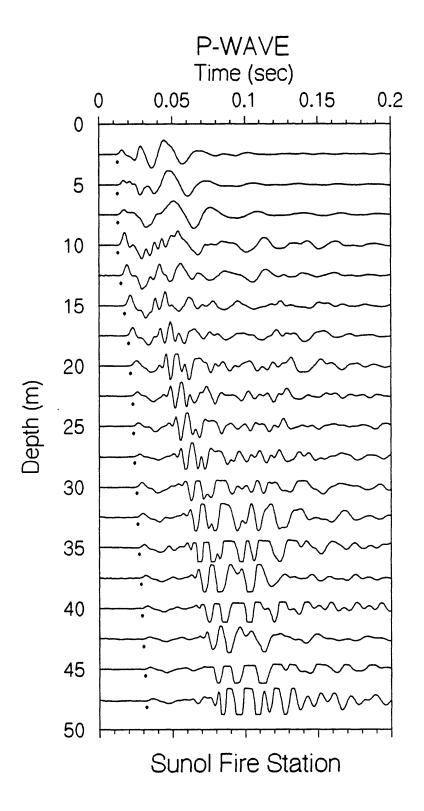


Figure 43. Vertical-component record section. P-wave arrivals are shown by the solid circles.

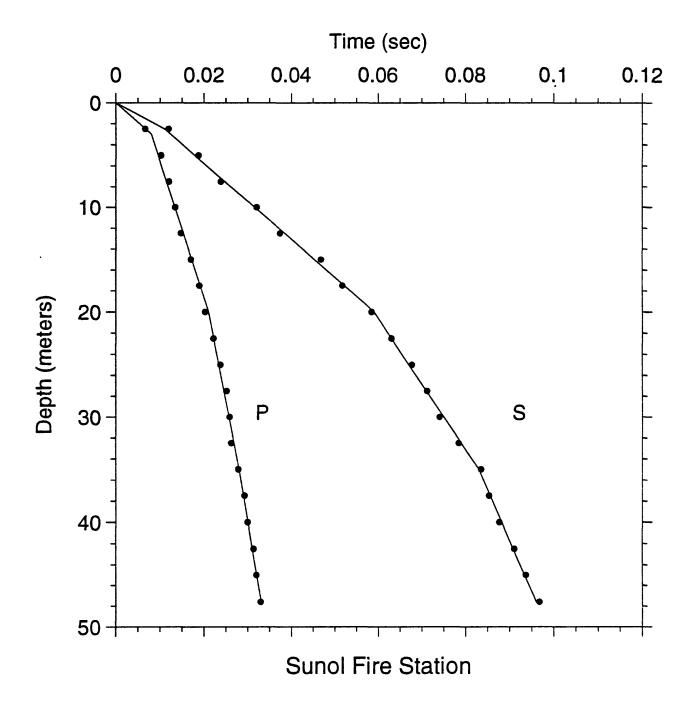


Figure 44. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

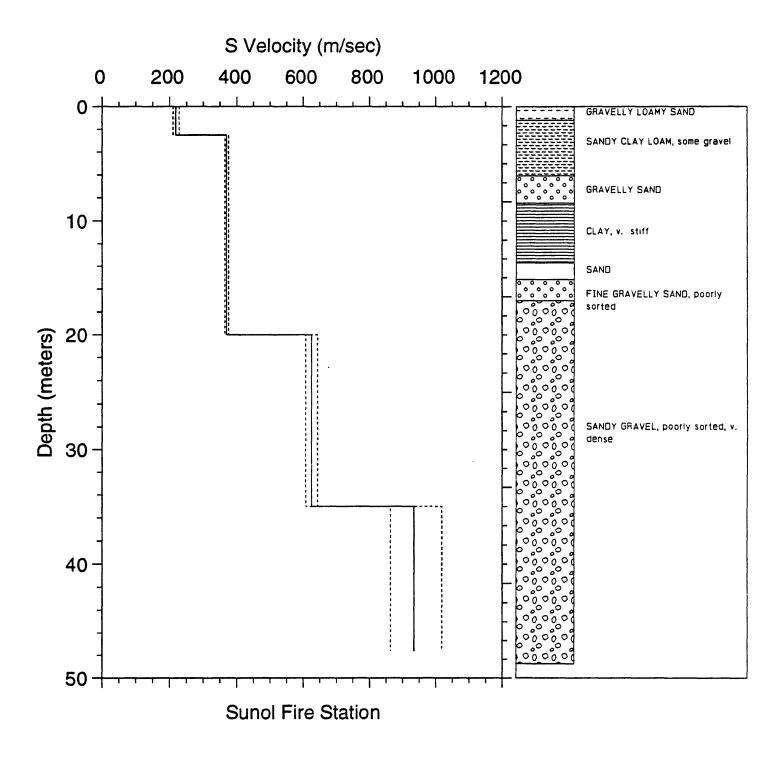


Figure 45. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

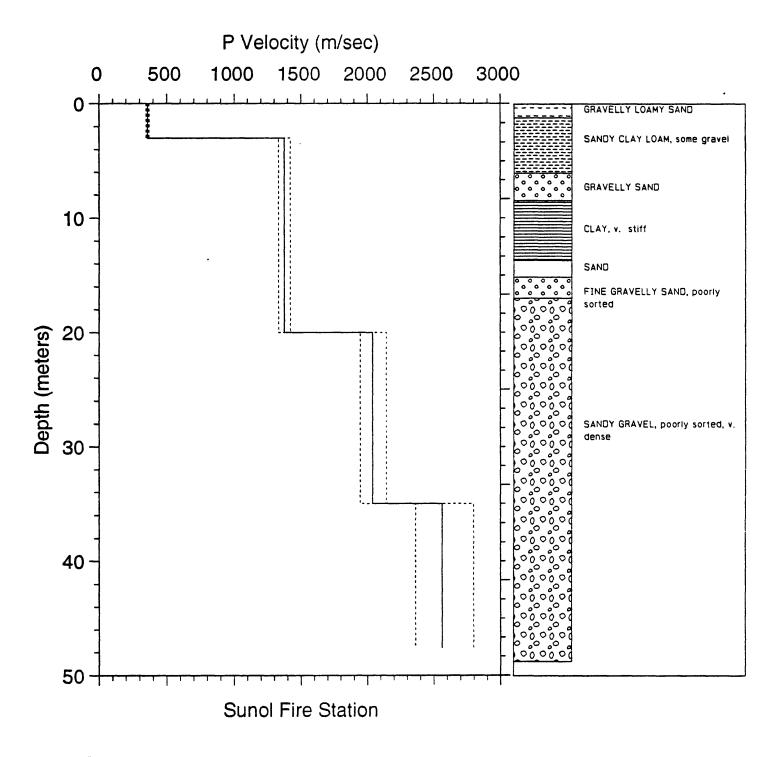


Figure 46. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

TABLE 9. S-wave arrival times and velocity summaries for Sunol Fire Station borehole.

vu(ft/s) 747 747 1230 2110 3339
688 688 688 1194 1993 2830
v(ft/s) 716 716 1212 2050 3063
vu(m/s) 228 228 275 375 1018
vt(m/s) 210 210 210 364 607 863
v(m/s) 218 218 218 369 369 625 934
ttb(s) .000 .011 .059 .083
dtb(ft) -0 8.2 65.6 114.8 156.2
dtb(m) 2.5 20.0 35.0 47.6
rsdl/sig
 92
t(sec) 119 .0119 .01187 .0238 .0320 .0373 .0468 .0517 .0712 .0740 .0770 .0770 .0784 .0835 .0835 .0835 .0936
4(ft) 16.4 16.4 17.8 17.8 17.8 17.8 17.8 17.8 17.8 17.8
d 23.5

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from

hammer blows differing in direction by 180°) sig = sigma, standard deviation normalized to the

ing — signia, standard deviation inclination standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet ttb(s) = arrival time in seconds to bottom of layer

U(n/s) = arrival time in seconds to bottom of v(m/s) = velocity in meters per second

v(m/s) = vectority in interest per second vectority) = lower limit of velocity in meters per second vector(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second
vu(ft/s) = upper limit of velocity in feet per second
\* see text for explanation of velocity limits

TABLE 10. P-wave arrival times and velocity summaries for Sunol Fire Station bore-

vu(ft/s) 1216 1216 1216 4661 7029 9181
(ft/s) 1141 1141 4372 6386 7749
v(ft/s) 1177 1177 4512 6692 8405
νυ(m/s) 371 371 1421 2143 2798
v((m/s) 348 348 1333 1946 2362
v(m/s) 359 359 1375 2040 2562
ttb(s) .000 .008 .021 .028 .033
dtb(ft) 9.8 65.6 114.8 156.2
dtb(m) 3.0 3.0 20.0 35.0 47.6
751 7
10066 0102 0102 01134 01147 01170 0202 02037 0258 0278 0278 0278 0278 0278 0278 0278
4(ft) 8.7.1 16.4 16.4 24.6 24.6 27.6 65.6 65.6 65.6 65.6 114.8 114.8 113.0 1133.0
6 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from

hammer blows differing in direction by 180°) sig = sigma, standard deviation normalized to the

ig = sigma, standard deviation normanize standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet ttb(s) = arrival time in seconds to bottom of layer

ttb(s) = arrival time in seconds to bottom or <math>v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second \* vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second <math>vu(ft/s) = upper limit of velocity in feet per second

\* see text for explanation of velocity limits

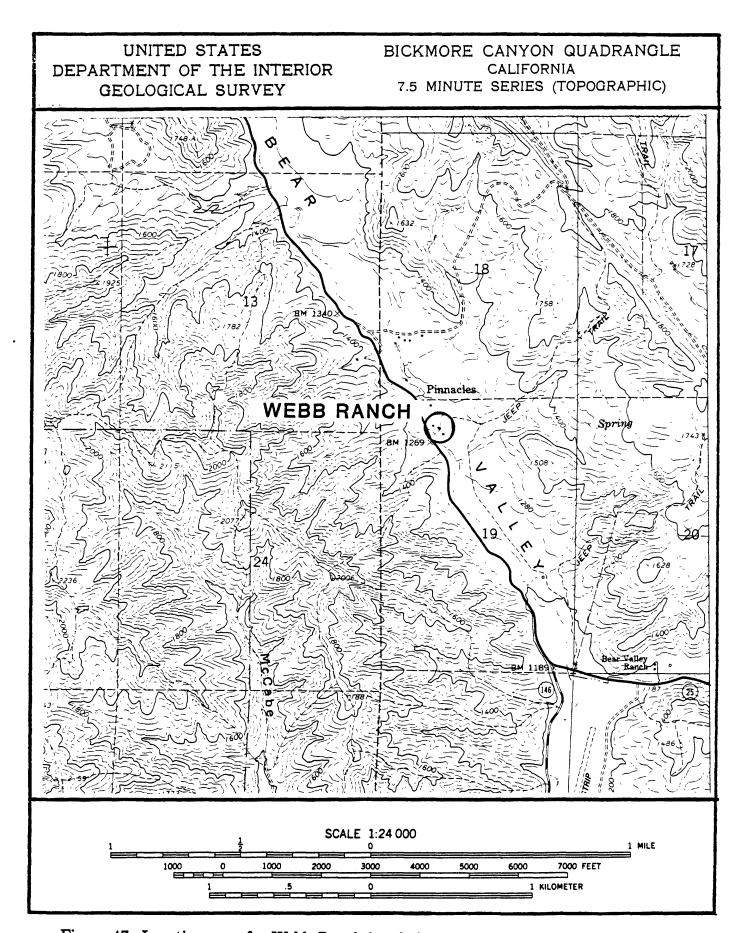


Figure 47. Location map for Webb Ranch borehole. The borehole is located approximately 30 meters from the strong-motion recorder.

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

<u>cm</u>	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	ciose
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

#### Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

discoloration

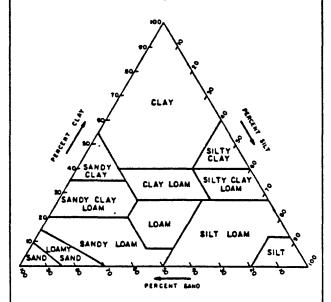
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough dis-

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

<u>blows/ft.</u>	relative <u>density</u>	<u>blows/ft.</u>	consistency		
0-4	v. loose	<2	v. soft		
4-10	loose	2-4	soft		
10-30	medium	4-8	medium		
30-50	dense	8-15	stiff		
>50	v. dense	15-30	v. stiff		
		>30	hard		

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

#### Types of samples

SP - Standard Penetration 1+3/8 in in ID sampler)

S - Thin-wall push sampler

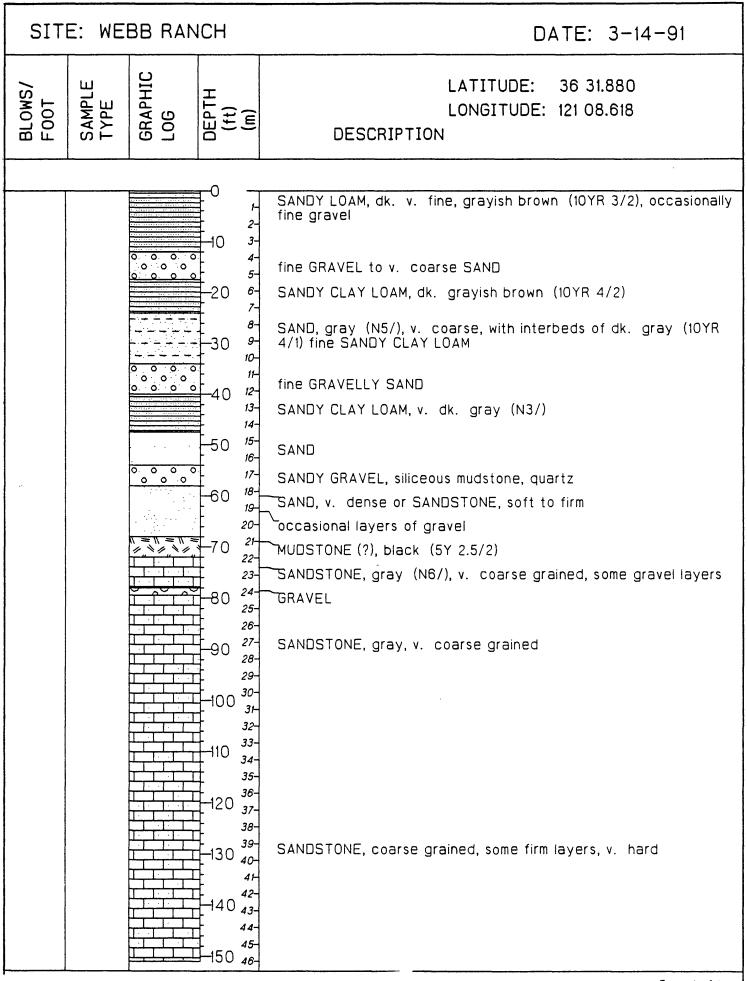
O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 48. Explanation of geologic log.



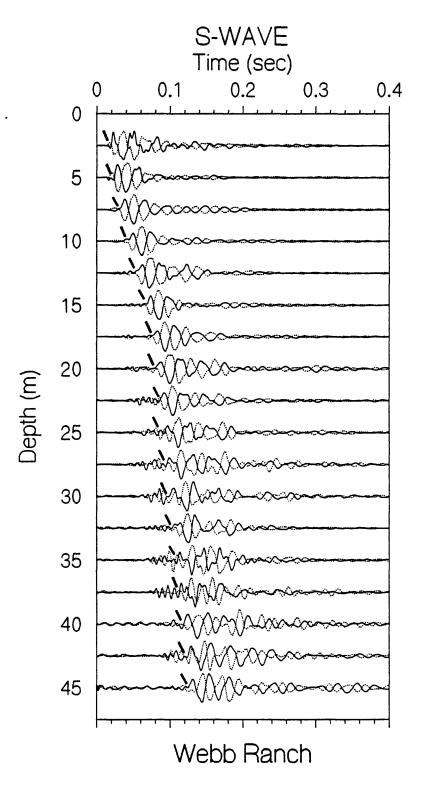


Figure 50. Horizontal-component record section (from horizontal impacts in opposite directions) superimposed for identification of S-wave onset. Approximate S-wave picks are indicated by the accent marks.

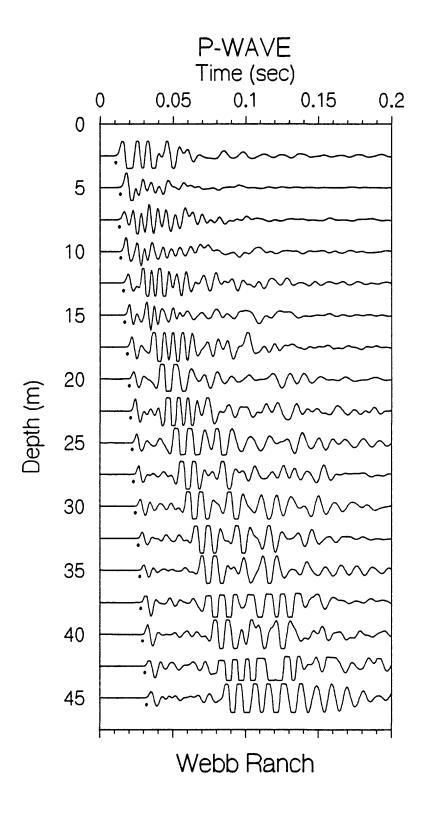


Figure 51. Vertical-component record section. P-wave arrivals are shown by the solid circles.

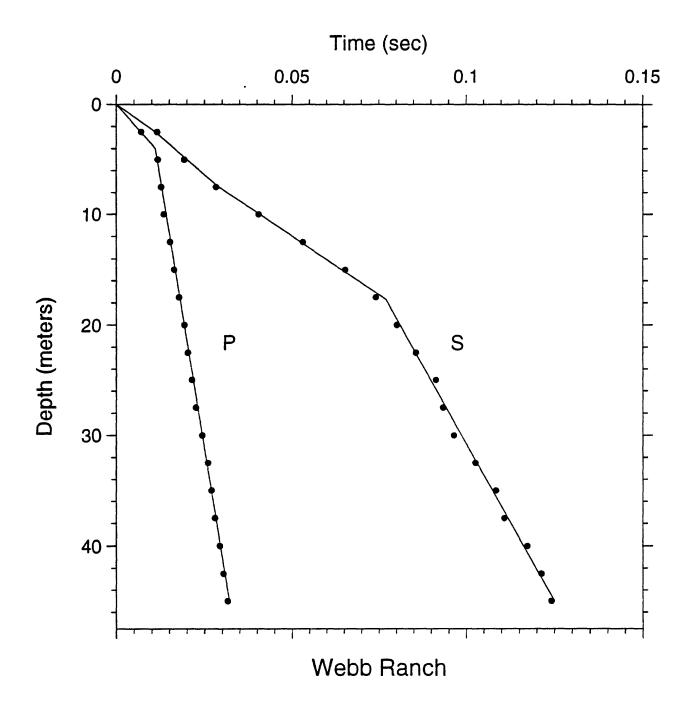


Figure 52. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

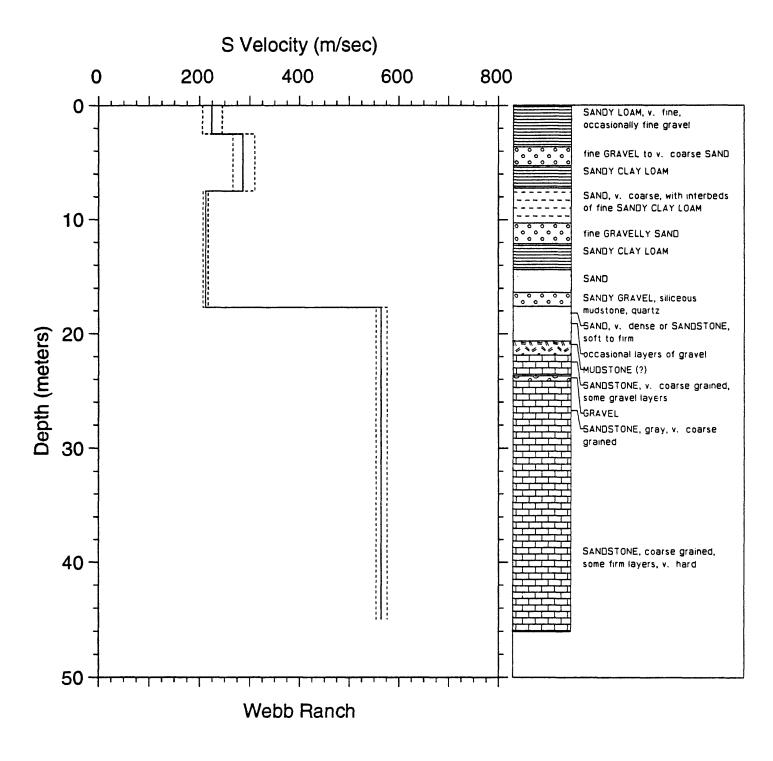


Figure 53. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

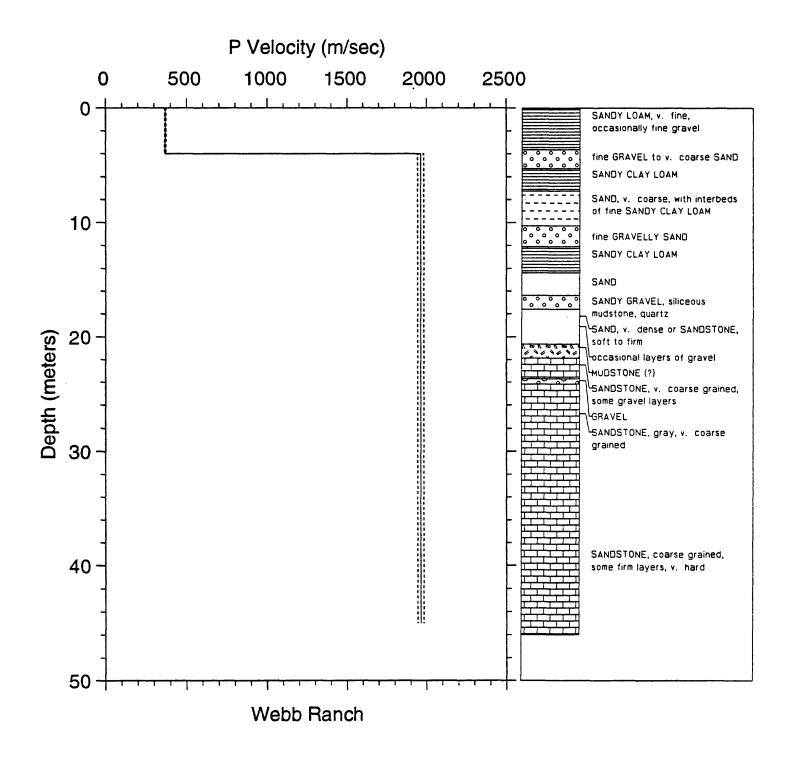


Figure 54. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

TABLE 11. S-wave arrival times and velocity summaries for Webb Ranch site.

w(ft/s) 805 805 1017 711 1888
v((ft/s) vu 676 676 873 881 1817
v(ft/s) 735 735 740 695 1852
vu(m/s) 245 245 310 310 576 576
v1(m/s) 206 206 266 207 554
V(m/s) 224 224 226 212 564 564
ttb(s) .000 .011 .029 .077
dtb(ft) .0 .8.2 24.6 58.1 147.6
dtb(m) 2.5 2.5 7.5 17.7 45.0
rsd(/sig
20 20 20 20 20 20 20 20 20 20 20 20 20 2
t(sec) 0115 0192 0192 0282 0741 0653 0741 0856 0934 0934 1026 1126 1133
d(ft) 16.4 16.4 16.4 32.8 32.8 441.0 65.6 77.4 73.8 82.0 98.4 114.8 1133.0 1133.4 147.6
4(a) 25.0 25.0 112.0 10 10 10 10 10 10 10 10 10 10 10 10 10

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma dtb(m) = depth to bottom of layer in meters dtb(ft) = depth to bottom of layer in feet

ttb(s) = arrival time in seconds to bottom of layer <math>v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second \* <math>vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second <math>vu(ft/s) = upper limit of velocity in feet per second

\* see text for explanation of velocity limits

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vl(m/s) = lower limit of velocity in meters per second \* vu(m/s) = upper limit of velocity in meters per second

ttb(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

vl(ft/s) = lower limit of velocity in feet per second <math>vu(ft/s) = upper limit of velocity in feet per second

v(ft/s) = velocity in feet per second

\* see text for explanation of velocity limits

TABLE 12. P-wave arrival times and velocity summaries for Webb Ranch site.

dtb(m) dtb(ft) ttb(s) v(m/s) vl(m/s) vu(ft/s) vl(ft/s) vu(ft/s) vu	Explanation:  d(m) = depth in meters d(ft) = depth in feet  t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°) sig = sigma, standard deviation normalized to the standard deviation of best picks rsdl/sig = least-squares residual divided by sigma
t(sec) sig rsdl/sig .0070 1.2 .0177 1.3 .0126 1.0 .0134 1.5 .0152 1.0 .0177 1.0 .0177 1.2 .0202 1.2 .0214 1.2 .0259 1.3 .0259 1.3 .0259 1.3 .0259 1.3	
 or	
(Sec.) 00170 01184 01184 01184 01184 01184 01883 01883 01883 01883 01883 01883 01883 01883 01883 01883	
Una de oua de oua de oua de	

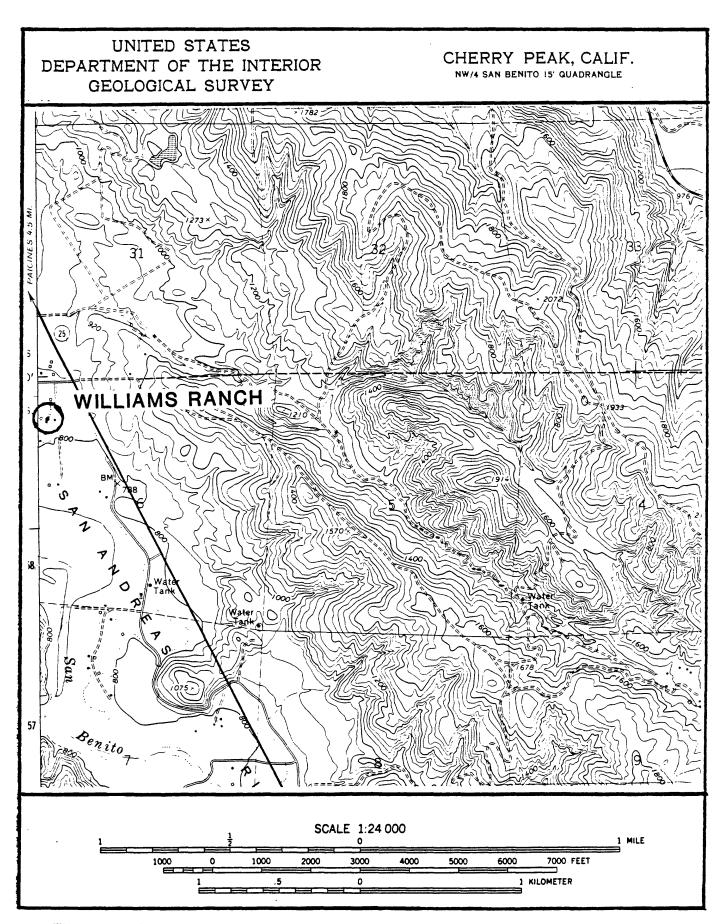


Figure 55. Site location map for Williams Ranch borehole. The borehole is located approximately 10 meters from the strong-motion recorder.

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

<u>cm</u>	in	fracture spacing
0-1	0-1/2	v. ciose
1-5	1/2-2	ciose
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

## Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

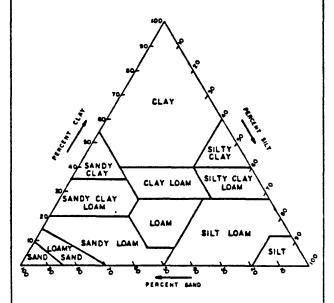
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

<u>blows/ft.</u>	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

## Types of samples

SP - Standard Penetration 1 + 3/8 in in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 56. Explanation of geologic log.

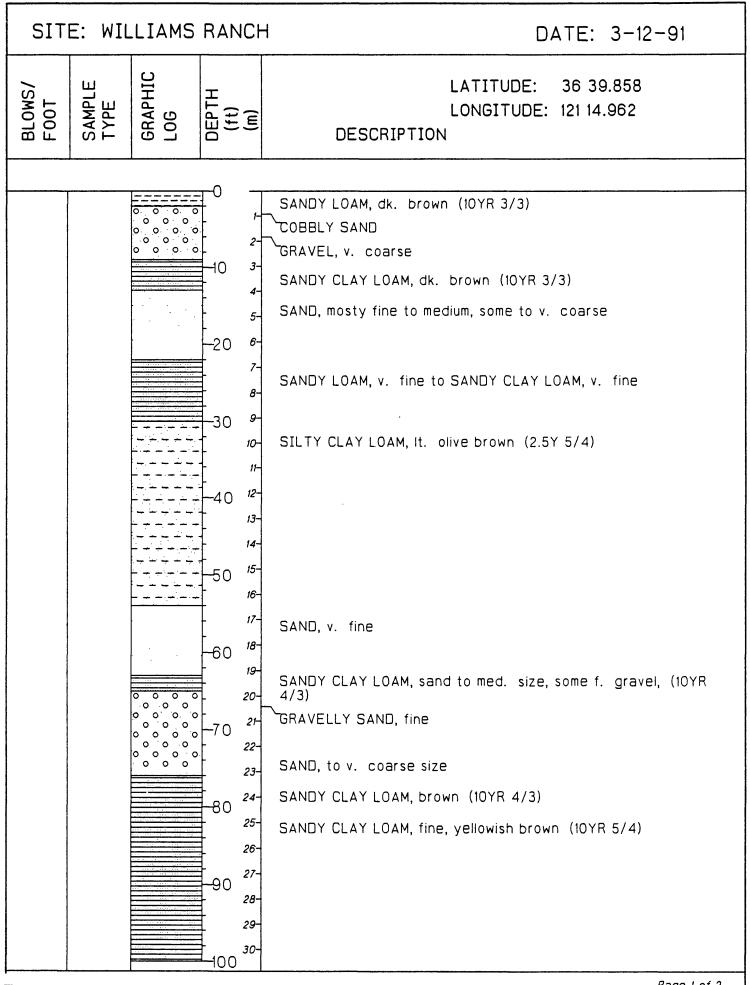
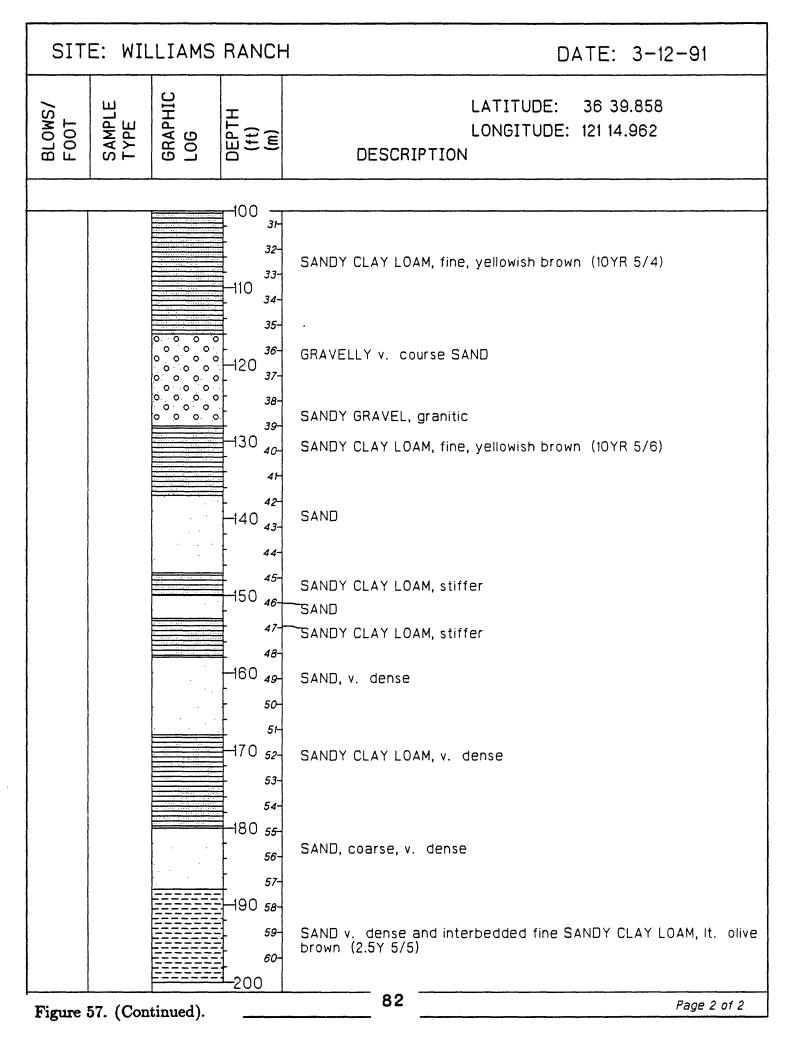


Figure 57. Geologic log of the Williams Ranch borehole.



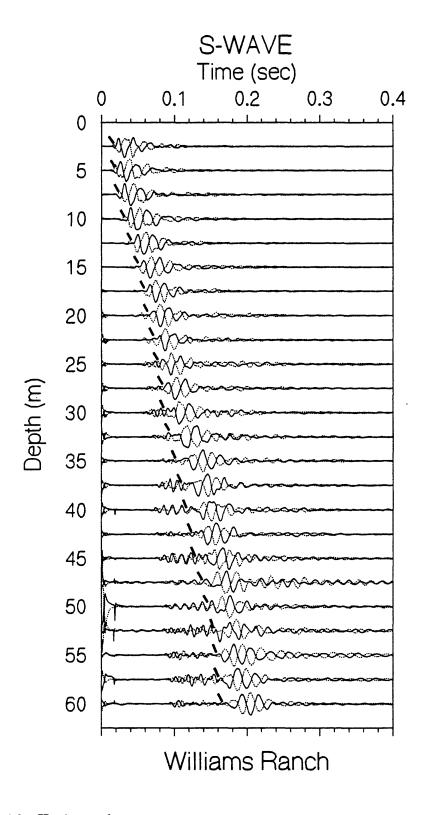


Figure 58. Horizontal-component record section (from horizontal impacts in opposite directions) superimposed for identification of S-wave onset. Approximate S-wave picks are indicated by the accent marks.

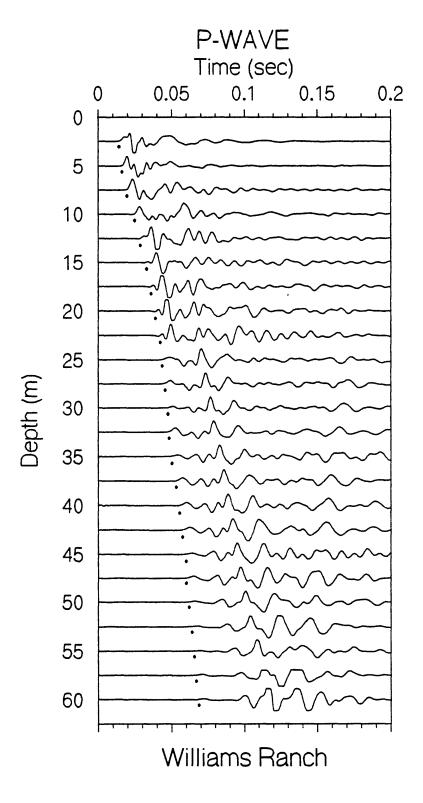


Figure 59. Vertical-component record section. P-wave arrivals are shown by the solid circles.

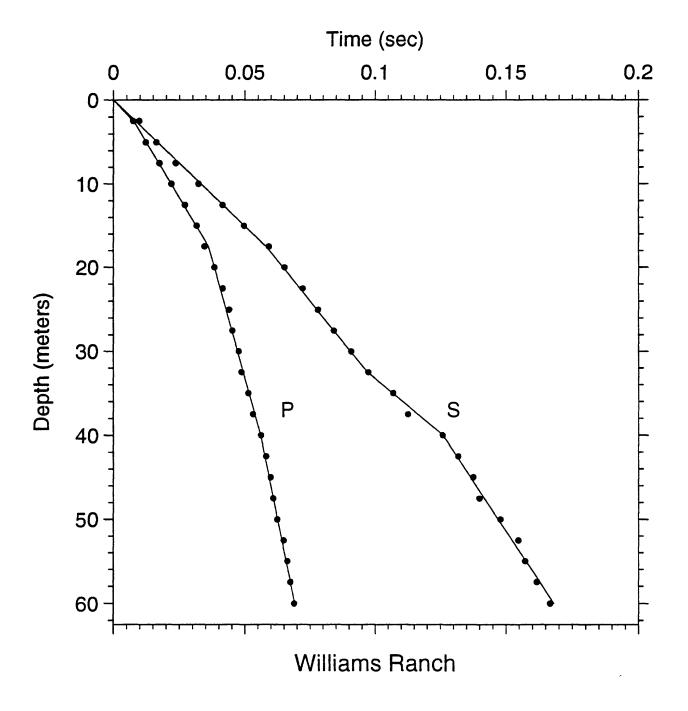


Figure 60. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

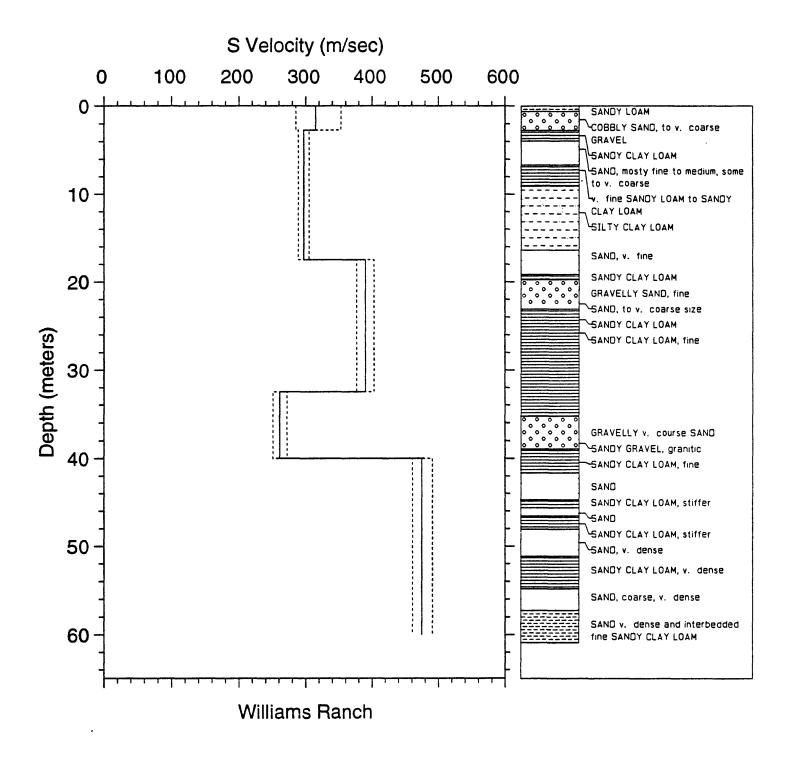


Figure 61. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

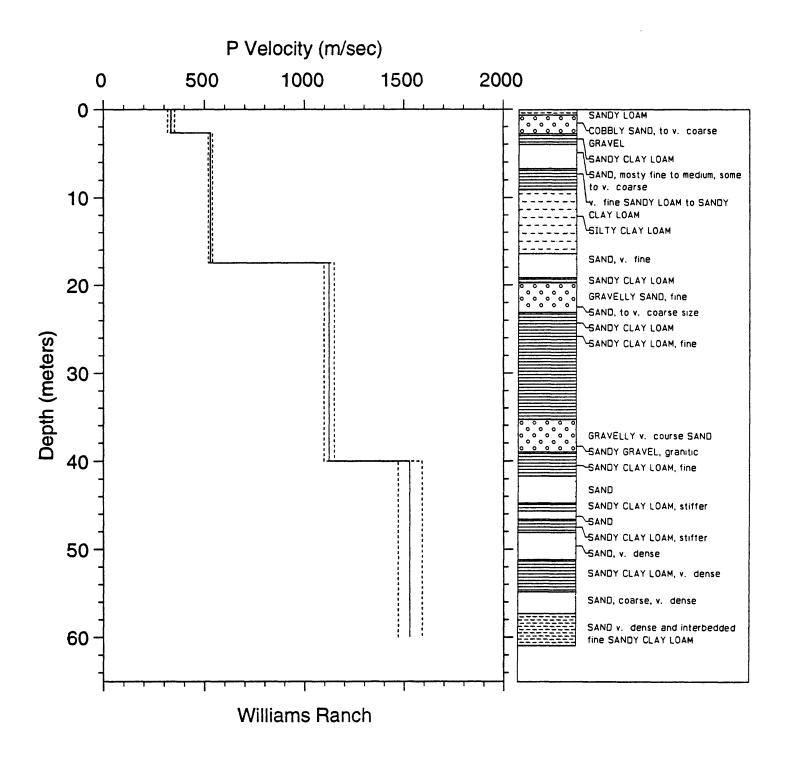


Figure 62. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. Simplified geologic log is shown for correlation with velocities.

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vu(ft/s) = upper limit of velocity in feet per second

\* see text for explanation of velocity limits

TABLE 13. S-wave arrival times and velocity summaries for Williams Ranch site.

				are	Ĕ								* .	ъ		
vu(ft/s) 1158 1158 1000 1321 894 1610				t(sec) = arrival time in seconds (S-wave arrival times are	the average of picks from traces obtained from	hammer blows differing in direction by 180°)	to the	e E	511 S 15		of layer		vl(m/s) = lower limit of velocity in meters per second *	vu(m/s) = upper limit of velocity in meters per second	•	second
v(ft/s) vl(ft/s) vu(ft/s) 1034 933 1158 1034 933 1158 973 947 1000 1278 1238 1321 857 822 894 1559 1512 1610				-wave arr	traces ob	n direction	sig = sigma, standard deviation normalized to the	standard deviation of best picks	tsut/sig = icast-squares residual unitida of significant of the squares of significant of the square	r in feet	ttb(s) = arrival time in seconds to bottom of layer	cond	n meters	in meters	<u>ب</u>	vl(ft/s) = lower limit of velocity in feet per second
v(ft/s) 1034 1034 973 1278 857 1559				conds (S	cks from	iffering i	riation n	of best p	n of lave	n of laye	conds to	ers per se	relocity i	velocity	per seco	elocity in
353 353 353 305 403 272 272 272		meters	feet	ime in se	age of pi	p swolq	dard dev	viation o	quares re to bottor	o botton	ime in se	y in mete	limit of \	· limit of	' in feet	imit of v
v((m/s) 285 285 289 377 251 251	•	d(m) = depth in meters	d(ft) = depth in feet	arrival t	the aver	hammer	ma, stan	standard deviation of best picks	- Icastra - denth	dtb(ft) = depth to bottom of layer in feet	arrival t	v(m/s) = velocity in meters per second	= lower	= upper	= velocity in feet per second	= lower l
v(m/s) 315 315 315 390 281 261 475	Explanation:	d(m) =	d(ft) = 0	t(sec) =	,		sig = sig	sta and I / nig	dth(m)	dtb(ft) =	ttb(s) =	v(m/s) :	vl(m/s)	vu(m/s)	v(ft/s) =	vl(ft/s)
.000 .009 .009 .058 .057 .126	Ex															
dtb(ft) .0 .0 8.9 8.9 57.4 106.6 131.2 196.9																
dtb(m) 2.7 17.5 32.5 40.0 60.0																
Sig rsd[/sig 1.1.1.1.3 1.1.2 1.1.3 1.0.3 1	2.6	6,	-1.2													
		<b>,</b> , ,	_													
	.1546	1616	1000													
		_														

455.50 60.50 6

TABLE 14. P-wave arrival times and velocity summaries for Williams Ranch site.

sig

dtb(m) dtb(ft) ttb(s) v(m/s) vu(m/s) vu(ft/s) vu	Explanation:  d(m) = depth in meters  d(ft) = depth in feet  t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)  sig = sigma, standard deviation normalized to the standard deviation of best picks  rsdl/sig = least-squares residual divided by sigma dtb(m) = depth to bottom of layer in meters dtb(ft) = depth to bottom of layer in feet ttb(s) = arrival time in seconds to bottom of layer v(m/s) = velocity in meters per second v(ft/s) = lower limit of velocity in meters per second v(ft/s) = velocity in feet per second v(ft/s) = lower limit of velocity in feet per second vu(ft/s) = upper limit of velocity in feet per second	* see text for explanation of velocity limits
18d(/sig	jwi4	